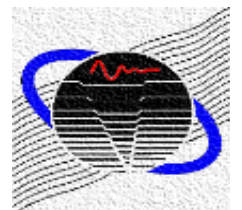


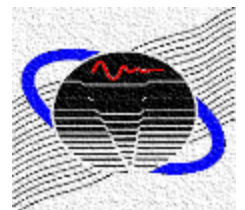
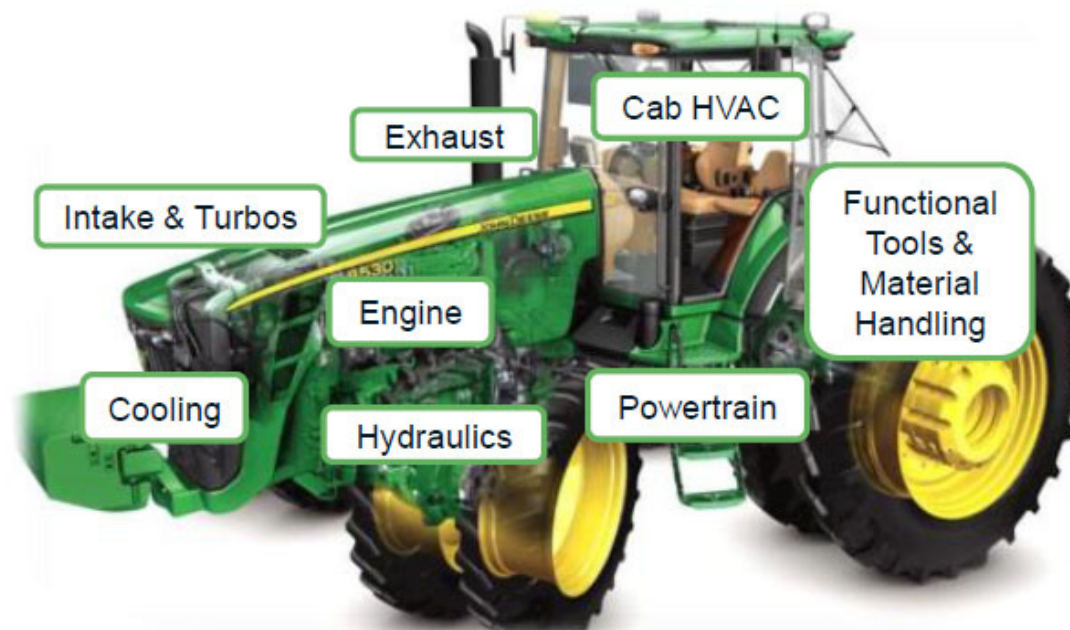
Hydraulic Fluidborne Noise Measurements

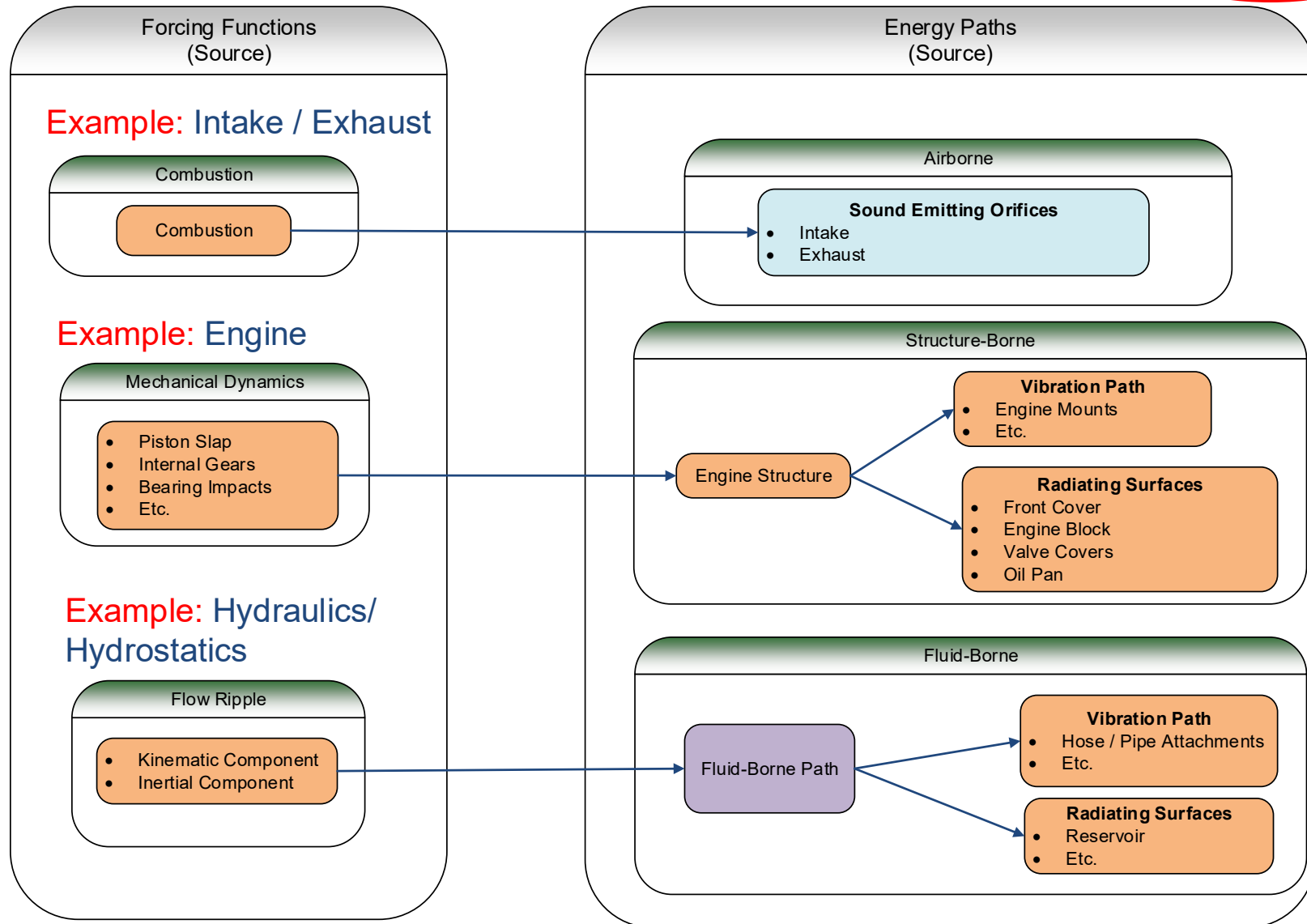
David Herrin
University of Kentucky

Vibro-Acoustics Consortium



Heavy Equipment Multiple Sources

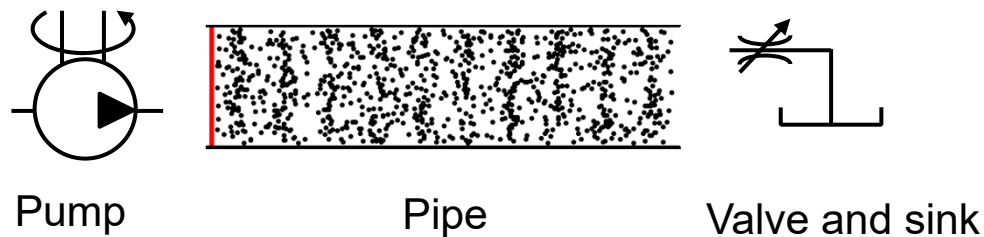




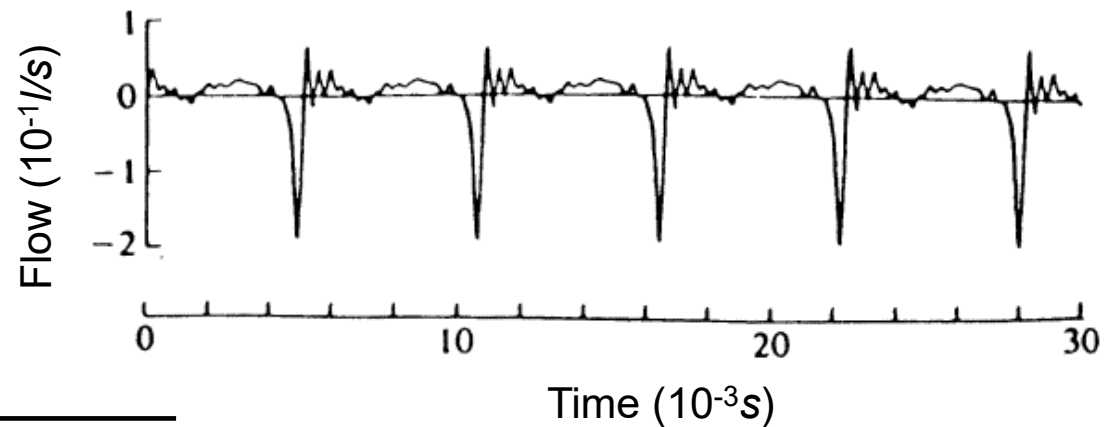
The source energy paths are characterized by the whether the forcing function is airborne, structure-borne, or Fluid-Borne.

Flow Ripple

- Kinematic Component
- Inertial Component



Typical flow ripple
for a piston pump:



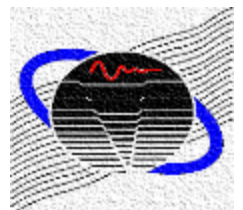
Standards

ISO 15086 Hydraulic fluid power – Determination of fluid-borne noise characteristics of components and systems

- ❖ Part 1 (2001): Plane wave model in hydraulics
- ❖ Part 2 (2000): Measurement of speed of sound
- ❖ Part 3 (2008): Measurement of hydraulic impedance

ISO 10767 Hydraulic fluid power – Determination of pressure ripple levels generated in systems and components

- ❖ Part 1 (1996): Measurement of source flow ripple and source impedance
- ❖ Part 1 (2015): Measurement of source flow ripple and source impedance



Plane Wave Model

Acoustic Pressure

$$P(x) = p_i e^{-jkx} + p_r e^{jkx}$$

$$k = \frac{2\pi f}{c}$$

Pressure Ripple

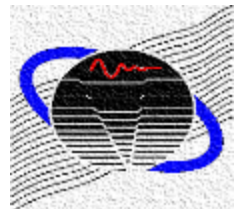
$$P(x) = p_i e^{-\gamma x} + p_r e^{\gamma x}$$

$$\gamma = j \frac{2\pi f}{c} \xi$$

ξ : viscosity coefficient

Viscosity Coefficient

$$\xi(\omega) \approx \left(1 + \sqrt{\frac{\nu}{2r_0^2 \omega}} \right) - j \left(\sqrt{\frac{\nu}{2r_0^2 \omega}} + \frac{\nu}{r_0^2 \omega} \right)$$



Plane Wave Model

Acoustic Particle Velocity

$$Q(x) = \frac{1}{Z_c} (p_i e^{-jkx} - p_r e^{jkx})$$

Flow Ripple

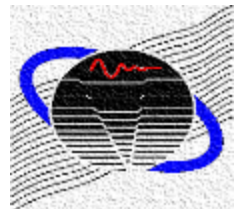
$$Q(x) = \frac{1}{Z_c} (p_i e^{-\gamma x} - p_r e^{\gamma x})$$

Characteristic Impedance

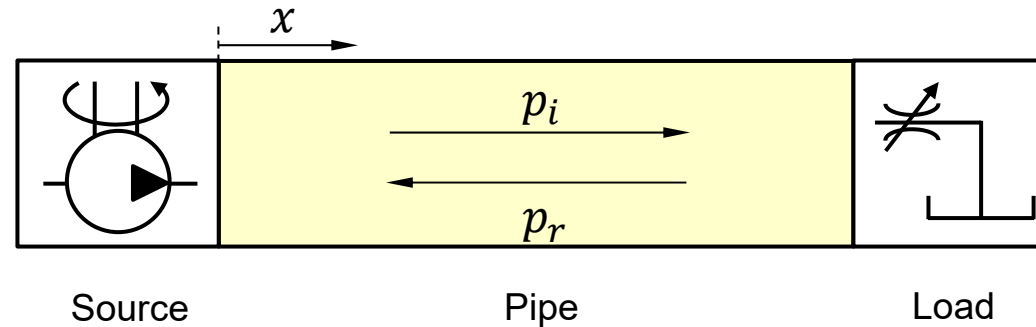
$$Z_c = \frac{\rho c}{S} \quad (\text{in air})$$

Characteristic Impedance

$$Z_c = \frac{\rho c \xi(\omega)}{S}$$



Plane Wave Model



$$P(x) = p_i e^{-\gamma x} + p_r e^{\gamma x}$$

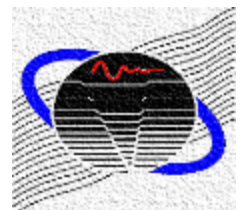
$P(x)$: fluid pressure at location x

p_i : incident wave amplitude

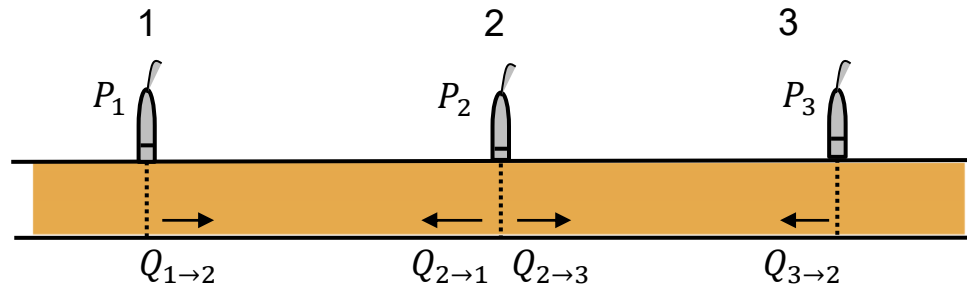
p_r : reflected wave amplitude

γ : wave propagation coefficient

x : location in the pipe



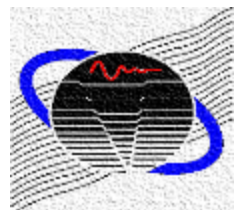
Hydraulic Transfer Matrix



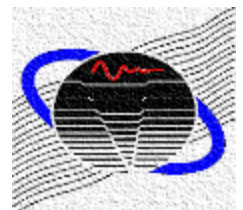
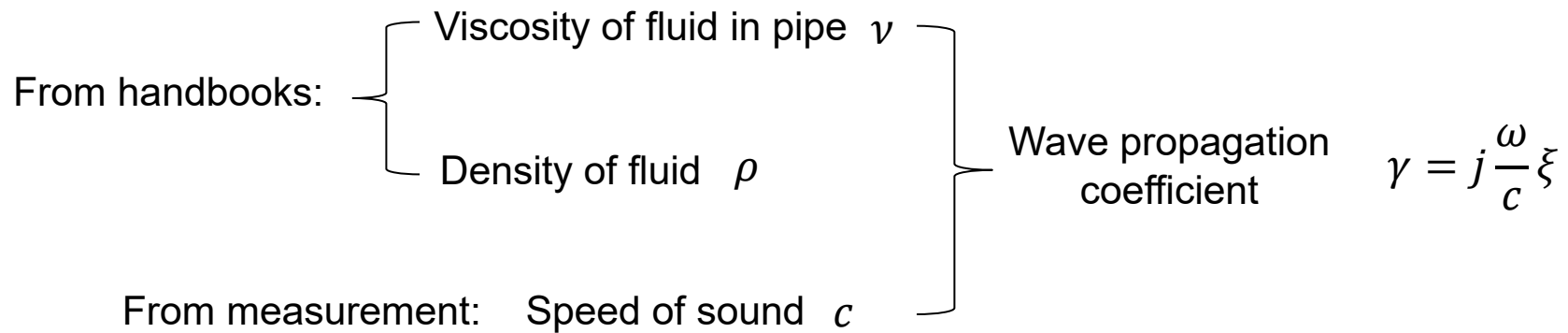
$$\begin{bmatrix} P_1 \\ Q_{1 \rightarrow 2} \end{bmatrix} = \begin{bmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{bmatrix} \begin{bmatrix} P_2 \\ Q_{2 \rightarrow 1} \end{bmatrix}$$

$$\begin{bmatrix} P_2 \\ Q_{2 \rightarrow 3} \end{bmatrix} = \begin{bmatrix} T_{22} & T_{23} \\ T_{32} & T_{33} \end{bmatrix} \begin{bmatrix} P_3 \\ Q_{3 \rightarrow 2} \end{bmatrix}$$

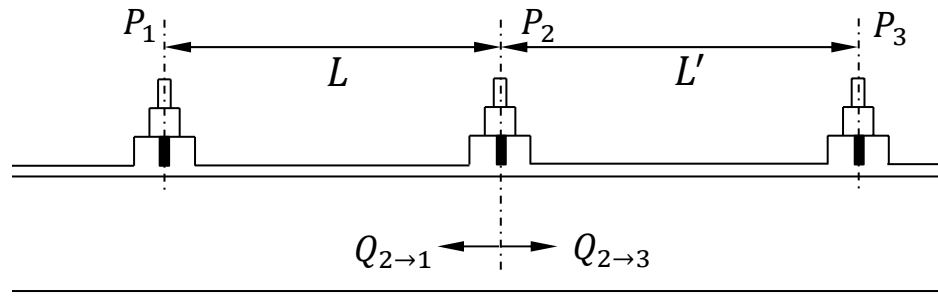
$$Q_{2 \rightarrow 1} + Q_{2 \rightarrow 3} = 0$$



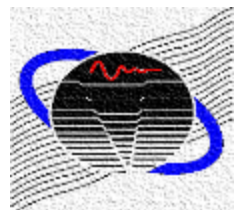
Property Calculations



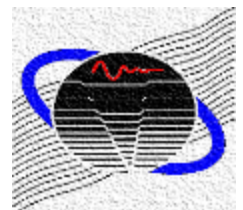
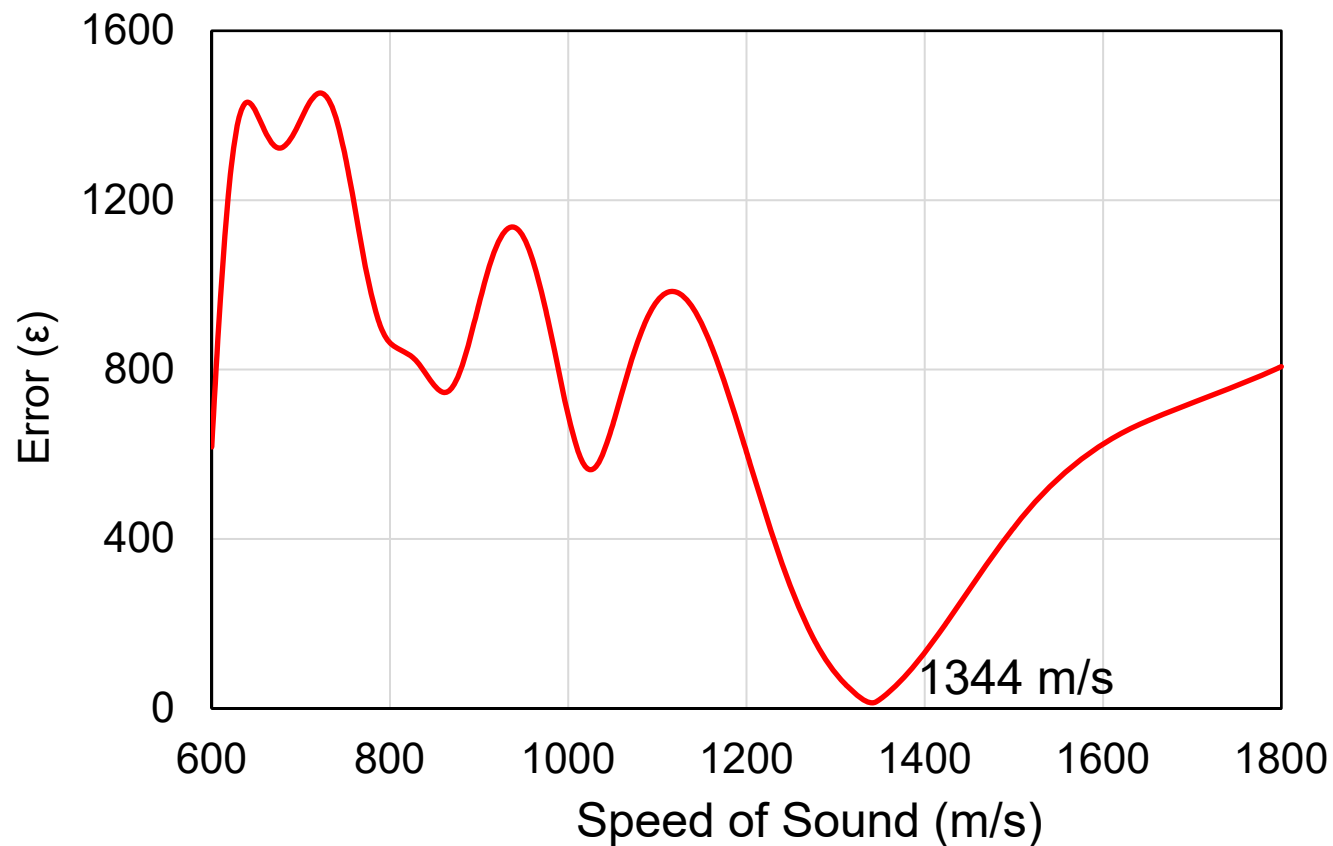
Speed of Sound ISO 15086-2



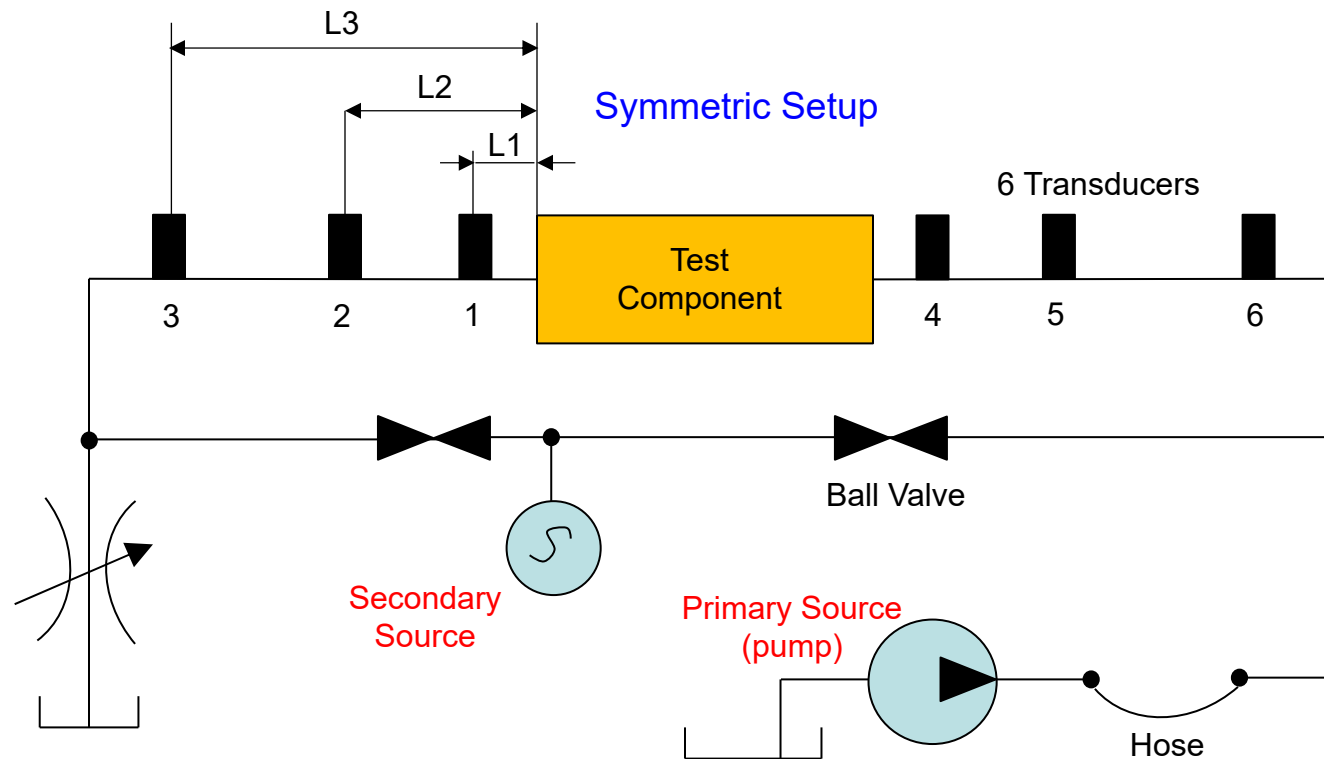
1. Assume speed of sound to determine incident and reflected wave using p_1 and p_2 .
2. Determine p_3 and compare to measured p_3 .
3. Iterate c until error is minimized.



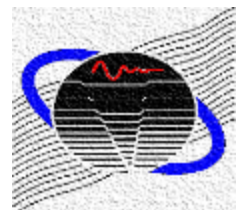
Speed of Sound ISO 15086-2



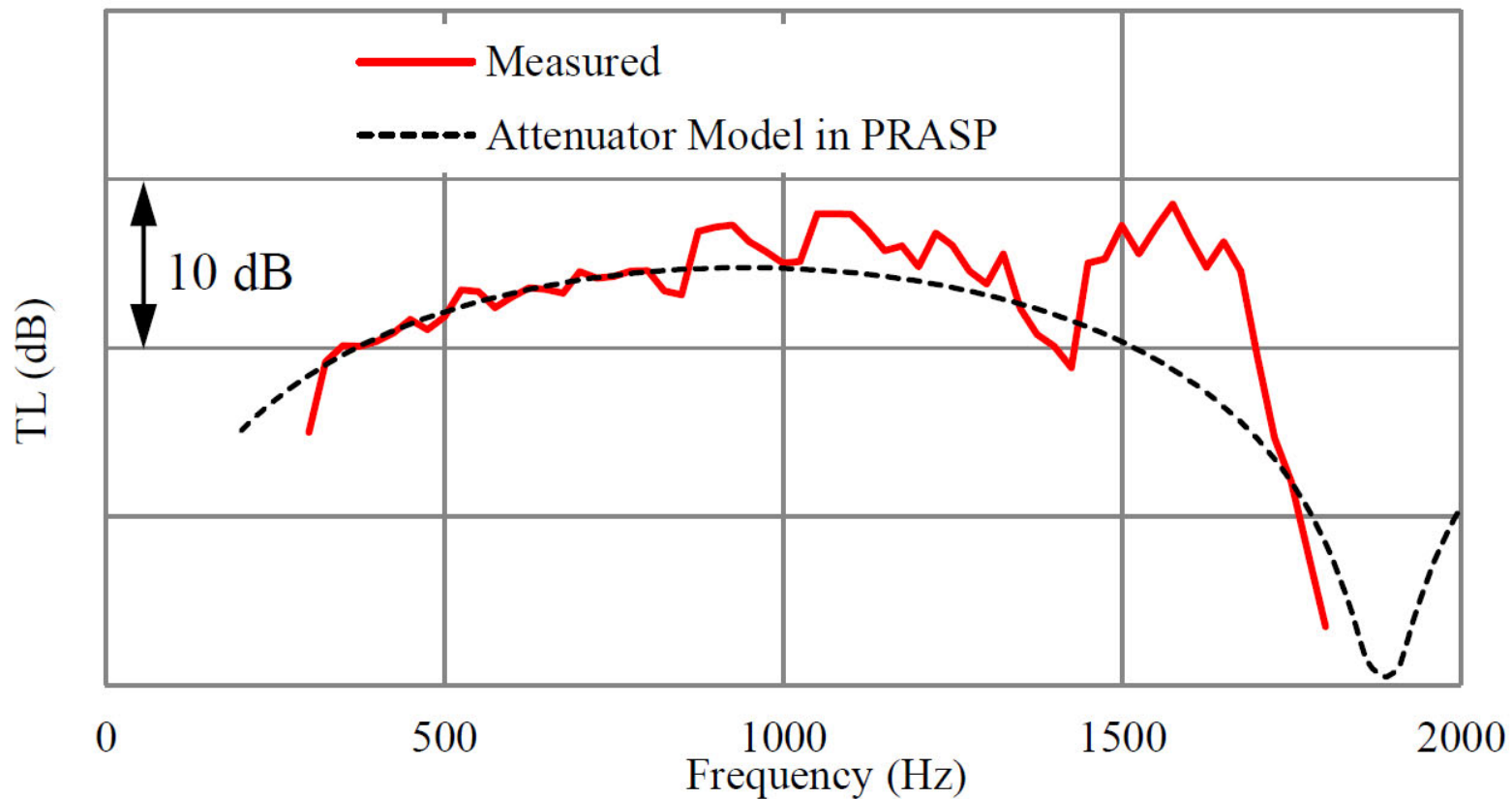
Transmission Loss Two Source Approach



Notes: primary pump is to provide the mean flow pressure and is running at 270 Hz.

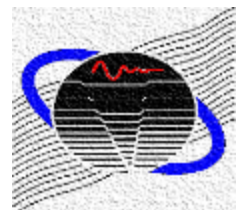


Transmission Loss ASTM E2611

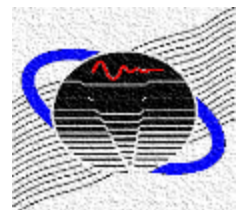
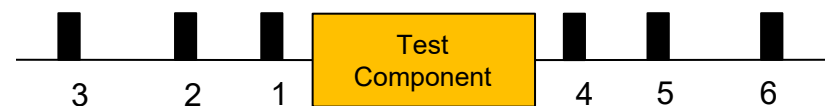
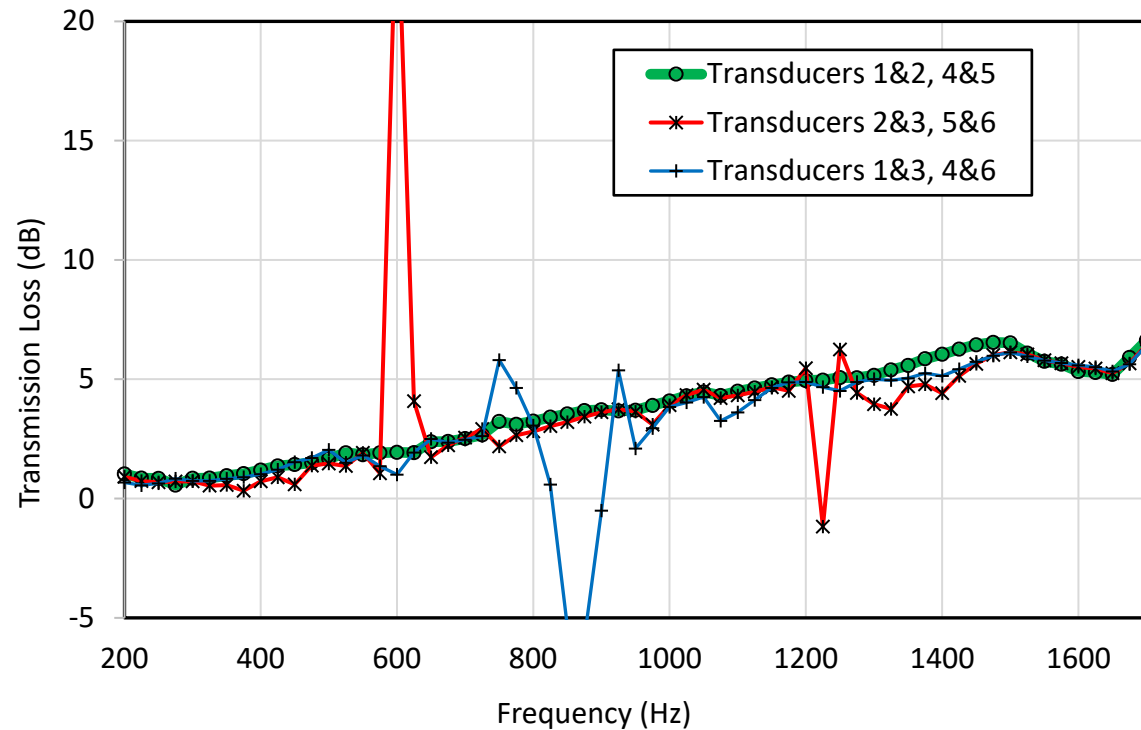


Liu, Suh, and Yang (2017)

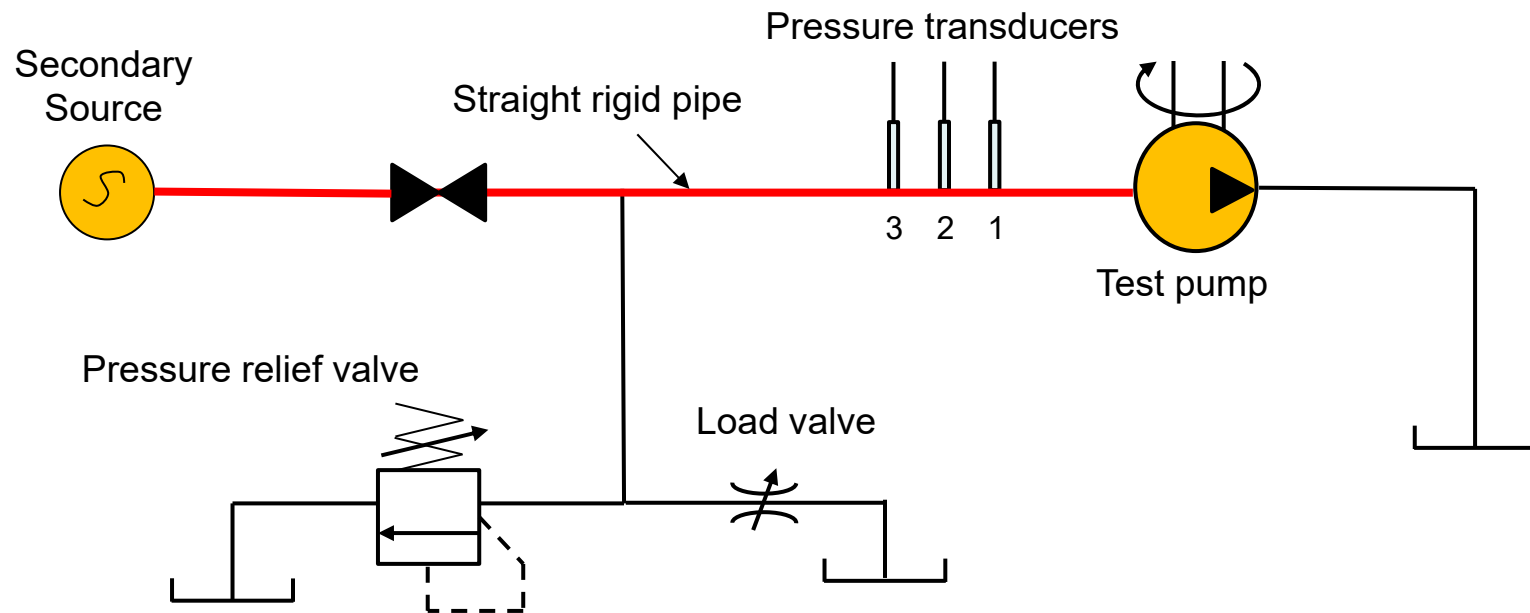
Vibro-Acoustics Consortium



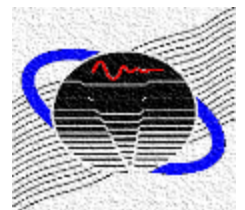
Transmission Loss ASTM E2611



Source Impedance ISO 10767-1 (1996)

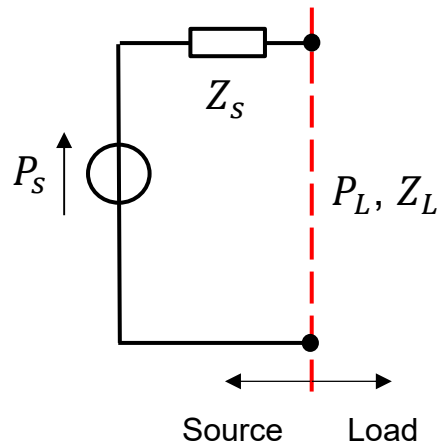


- More than 2 pressure transducers can be used for accuracy.
- Q_S and Z_S are solved at the harmonics of the secondary source.



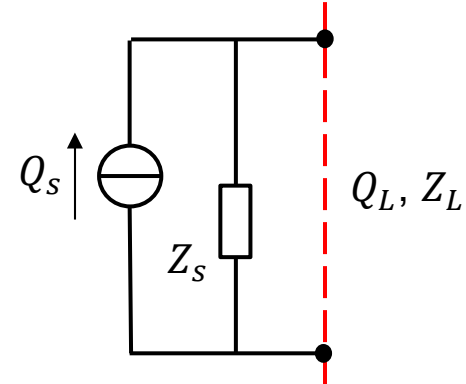
Source Impedance ISO 10767-1

Voltage source: P_s and Z_s

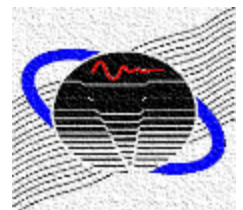


$$\frac{P_s}{Z_s + Z_L} = \frac{P_L}{Z_L}$$

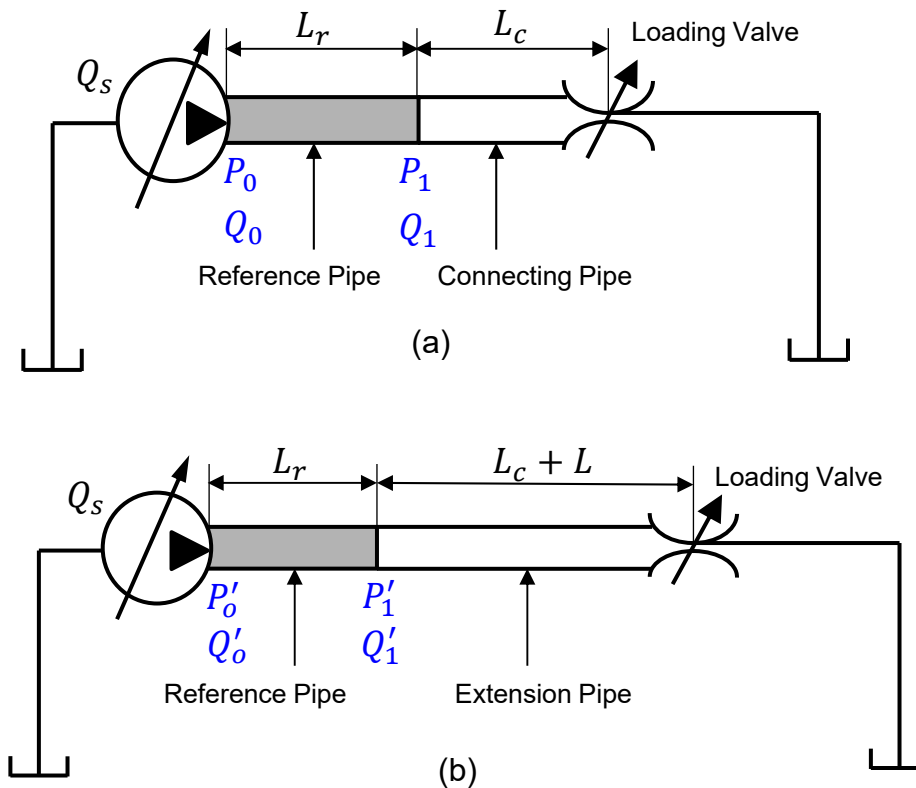
Current source: Q_s and Z_s



$$Q_s \frac{Z_s}{Z_s + Z_L} = Q_L$$



Source Impedance ISO 10767-1



$$Q_s - \frac{P_0}{Z_s} = Q_0$$

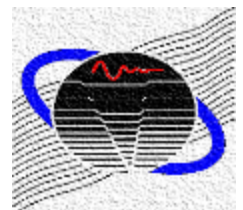
$$\begin{bmatrix} 1 & -P_{L1} \\ 1 & -P_{L2} \end{bmatrix} \begin{Bmatrix} Q_s \\ Y_s \end{Bmatrix} = \begin{Bmatrix} Q_{L1} \\ Q_{L2} \end{Bmatrix}$$

$$\text{Where } Y_s = 1/Z_s$$

Multi-load approach can be used, and source properties can be solved by least square approach.

Liu, Suh, and Butts (2018)

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Source Impedance Load Selection

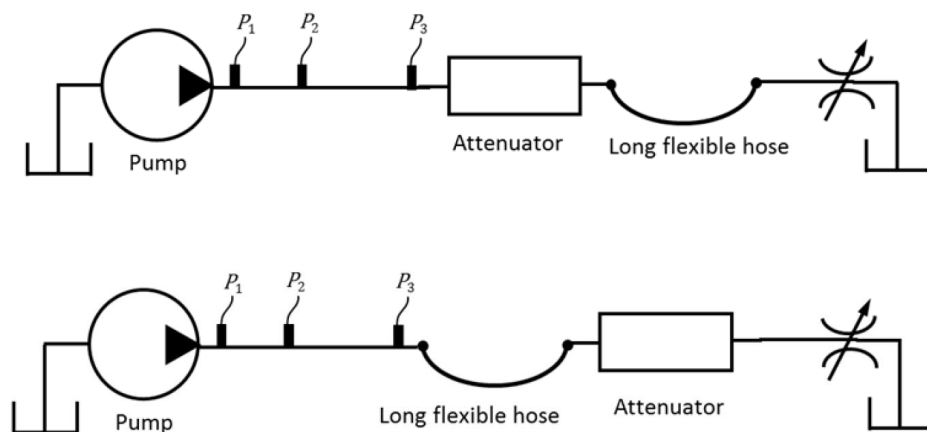


Fig. 2 – Modified Two-pressure/two-system Test Setup.

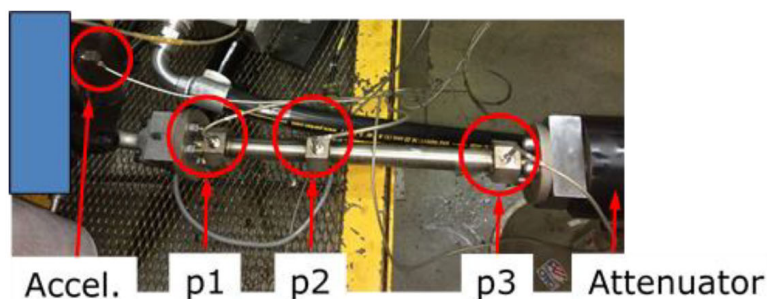
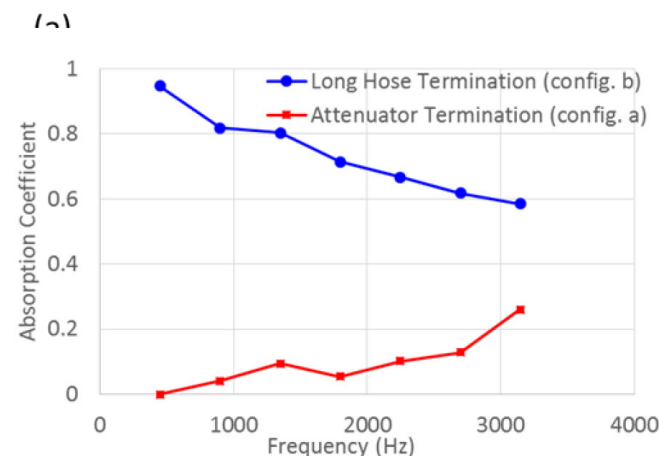
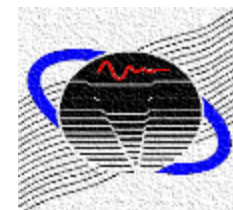


Fig. 3 – Physical Test Setup for Modified two-pressure/two-system configuration (a).



Liu, Suh, and Butts (2018)

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Source Impedance ISO 10767-1

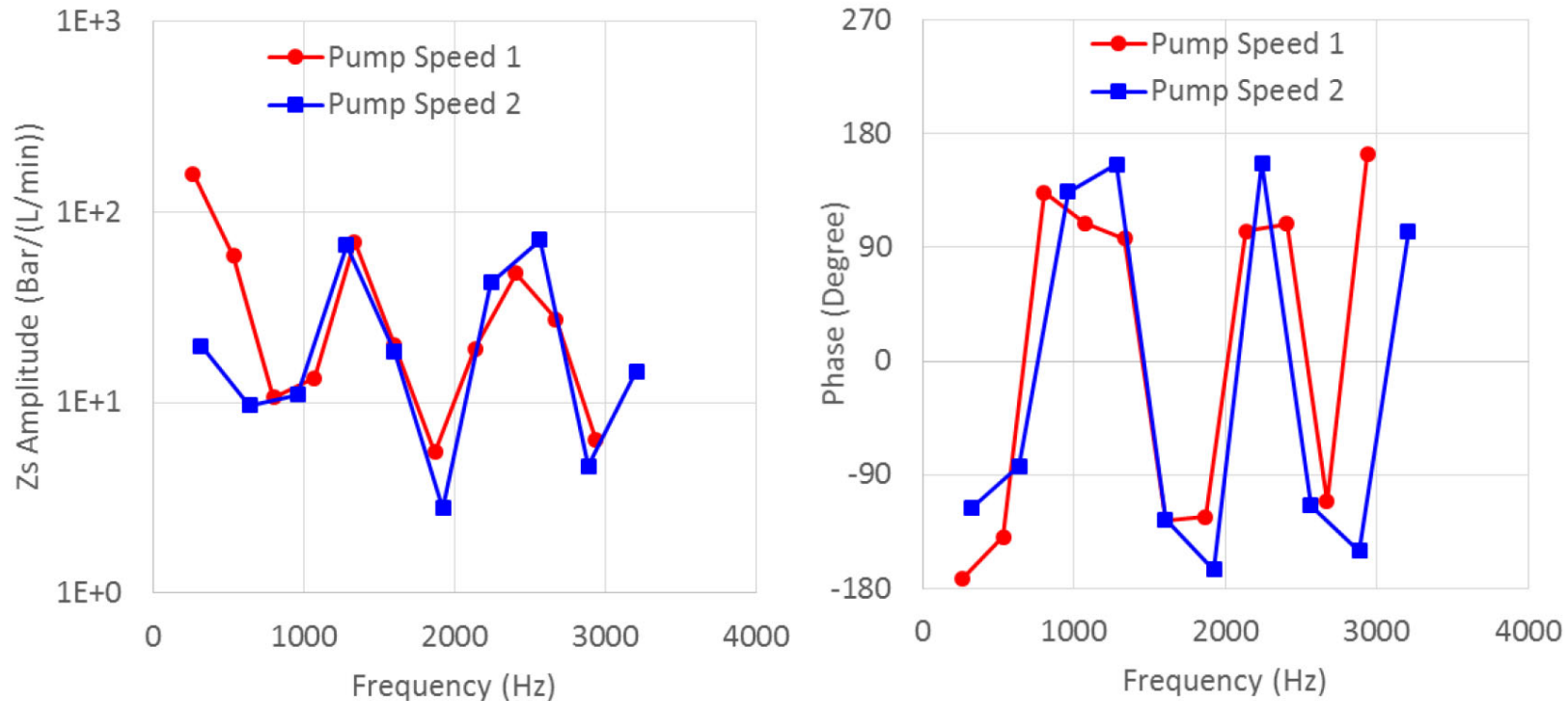
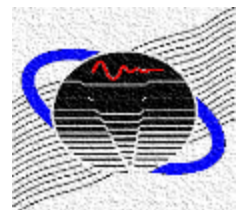


Fig. 6 – Pump impedance amplitude (left) and phase (right) measured under two different pump speeds.

Liu, Suh, and Butts (2018)

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Flow Ripple ISO 10767-1

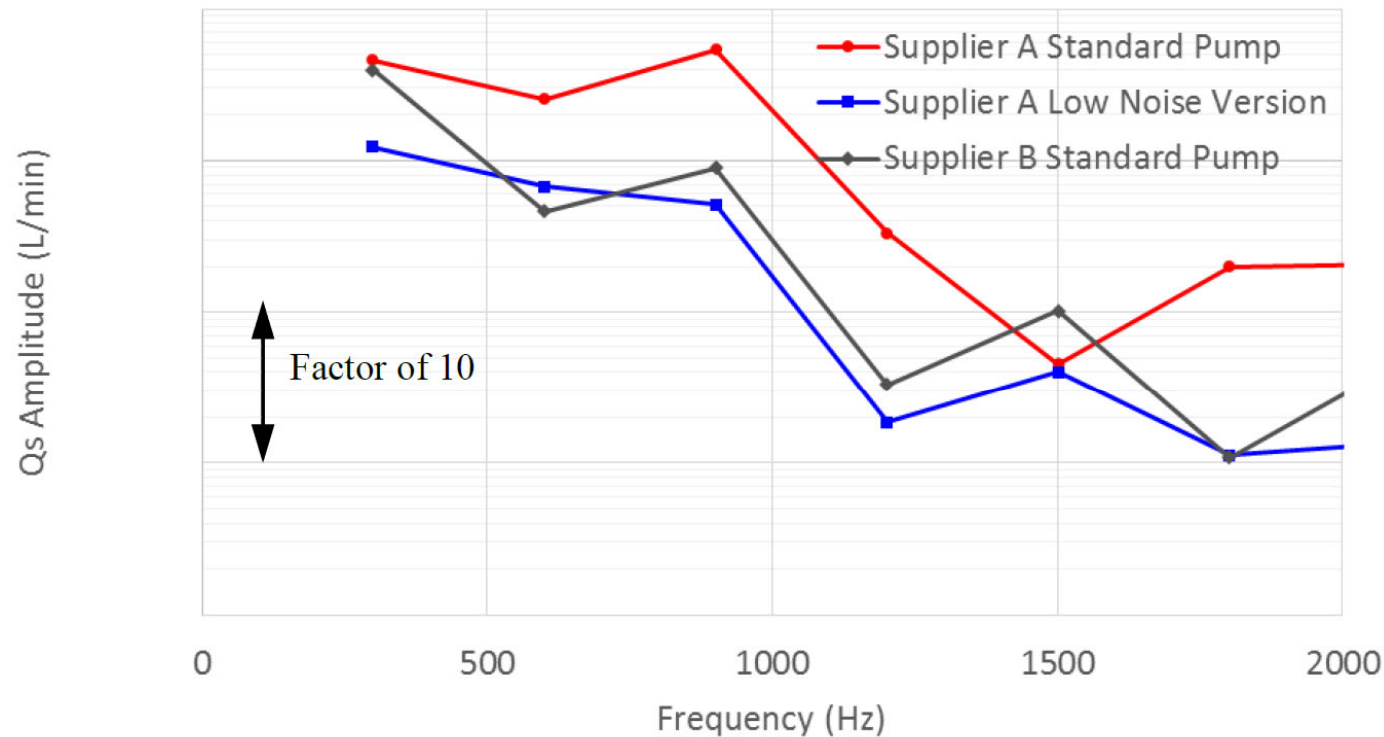
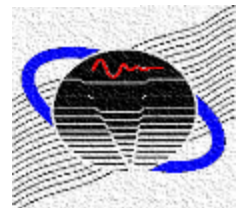


Fig. 9 – Pump flow rippled measured at medium pressure and medium speed condition.

Liu, Suh, and Butts (2018)

Vibro-Acoustics Consortium



Flow Ripple ISO 10767-1

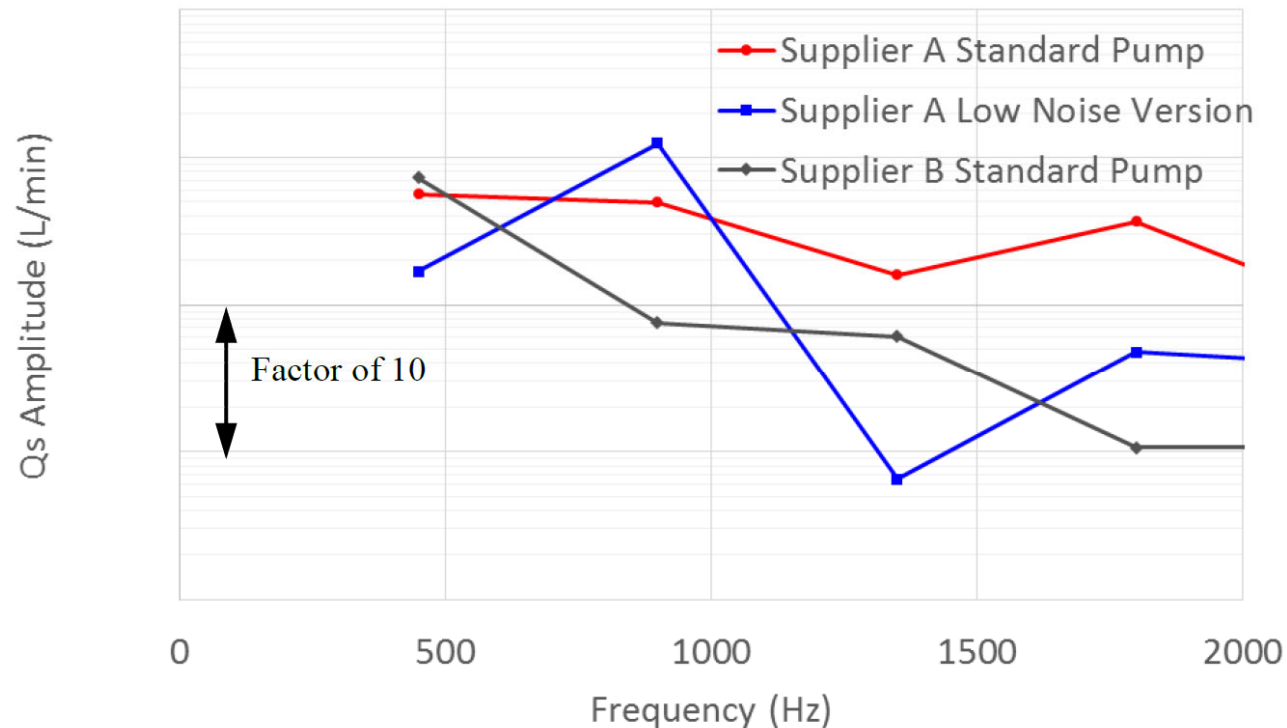
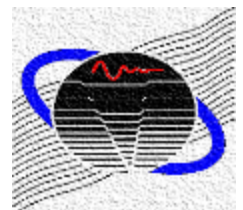


Fig. 10 – Pump flow rippled measured at maximum pressure and maximum speed condition.

Liu, Suh, and Butts (2018)

Vibro-Acoustics Consortium



References

- J. Liu, S. Suh, and Y. Yang, Hydraulic Fluid-borne Noise Measurement and Simulation for Off-Highway Equipment, *Noise-Con*, Grand Rapids, MI, June 12-14 (2017).
- J. Liu, S. Suh, and T. Butts, Source Flow Ripple and Source Impedance Measurement for Different Hydraulic Pumps, *Inter-Noise*, Chicago, IL, August 26-29 (2018).

