

December 17, 2020

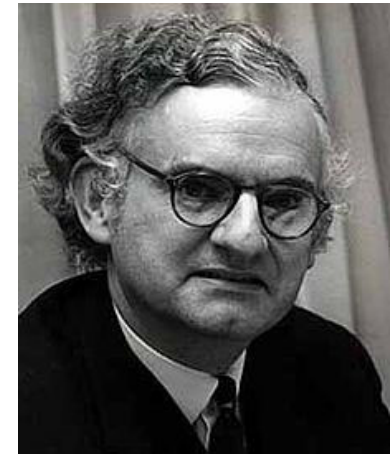
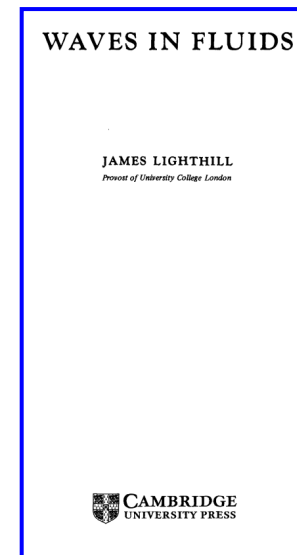
Flow Noise

Vibro-Acoustics Consortium Web Meeting
University of Kentucky

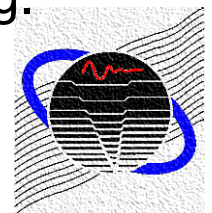
Lighthill's Analogy

Assumed only three fundamental types of sources are possible in a fluid.

- Monopole
- Dipole
- Quadrupoles

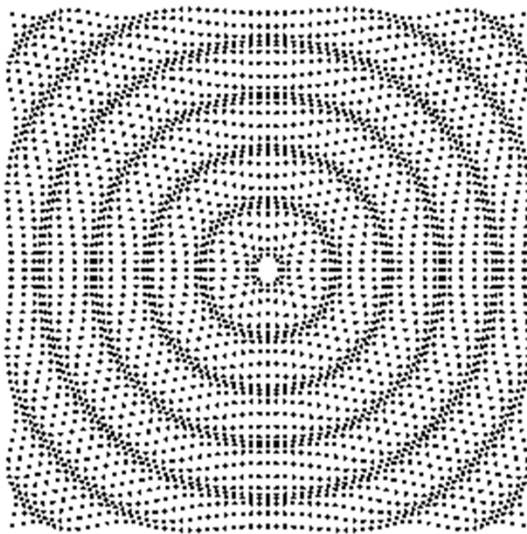


Weakness It ignores the interaction between sound and flow. An important example is the *whistle sound* caused by vortex shedding.

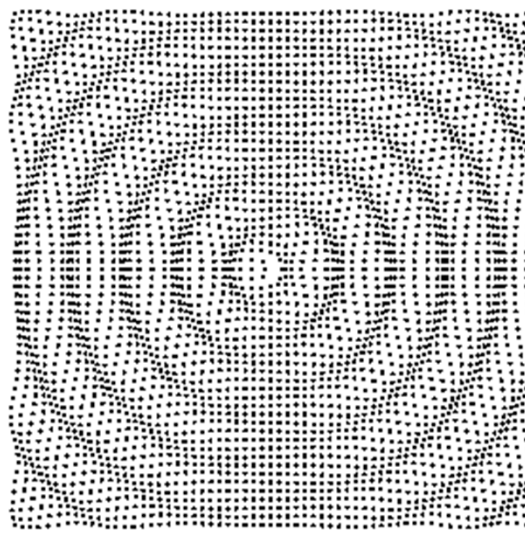


Elementary Sources

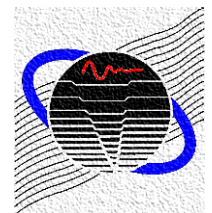
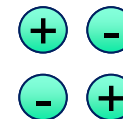
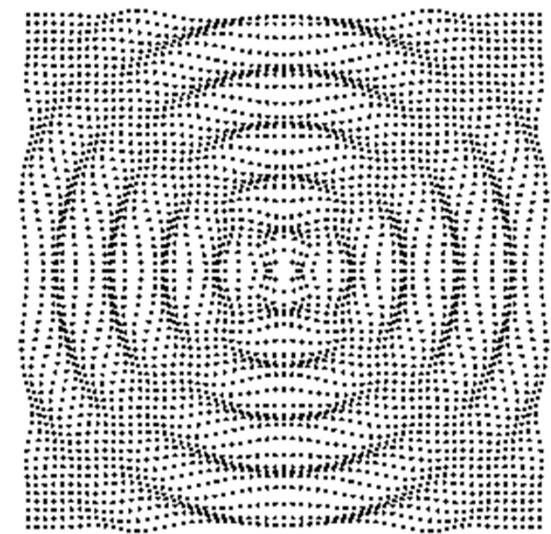
Monopole



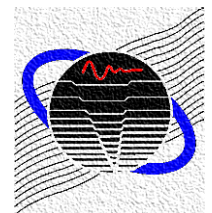
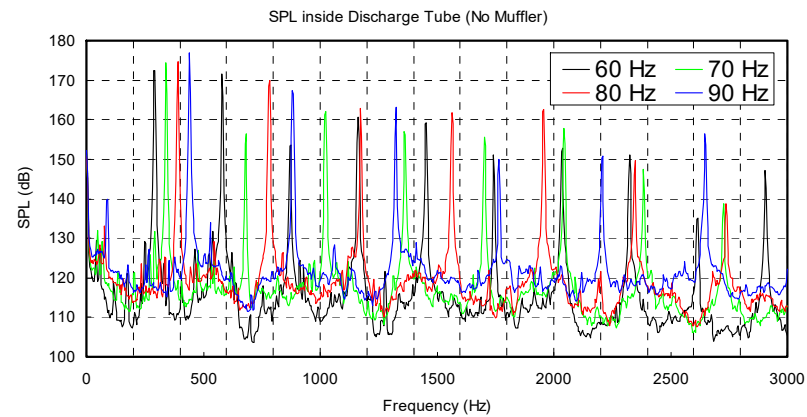
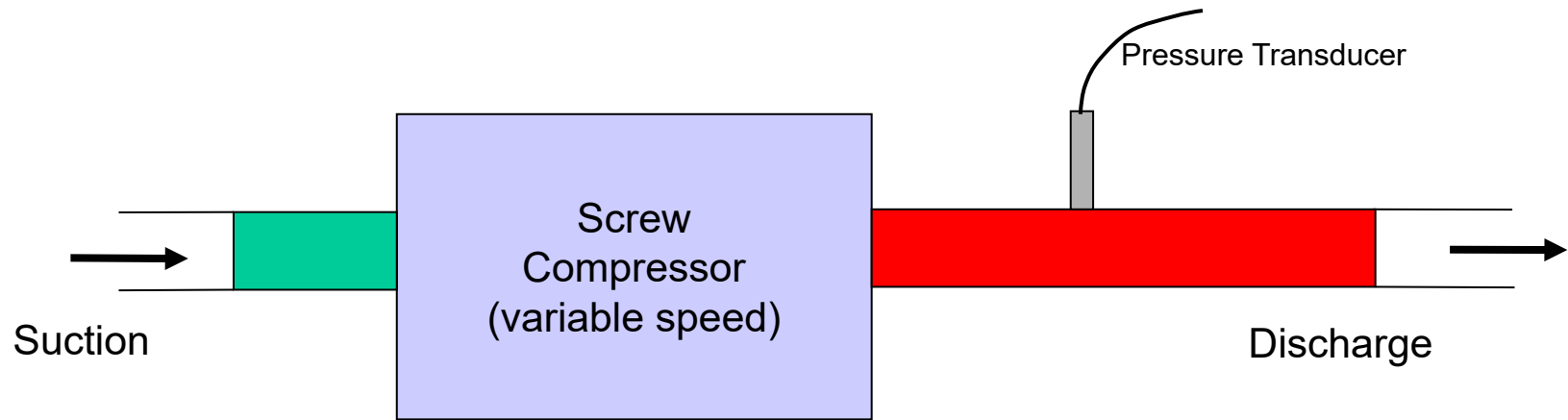
Dipole



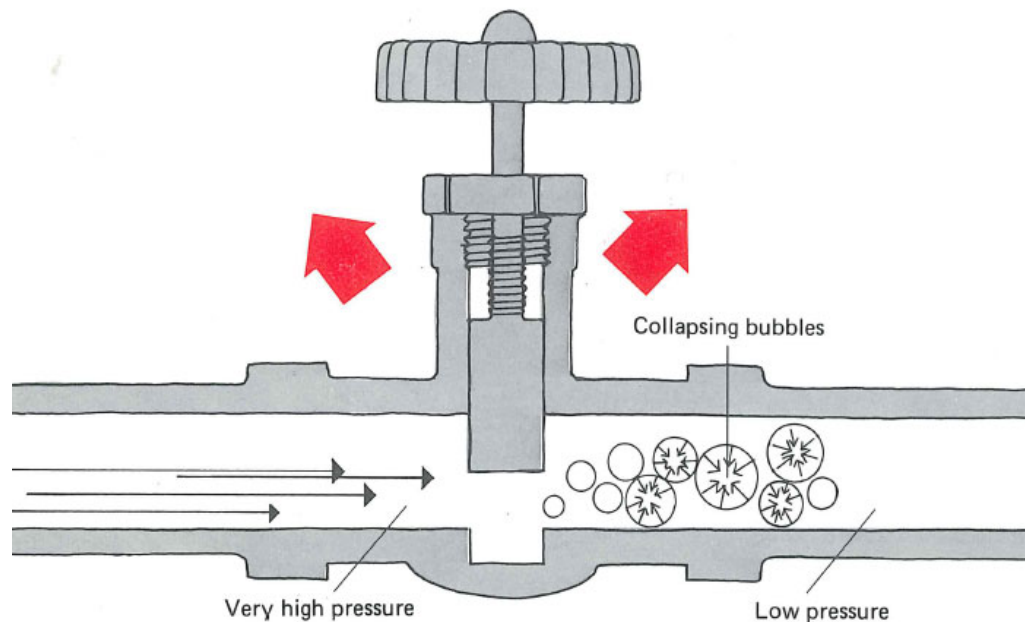
Quadrupole



Flow Noise Sources **Monopoles**

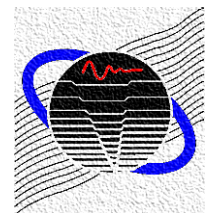


Flow Noise Sources **Monopoles**

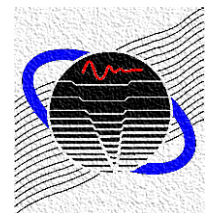
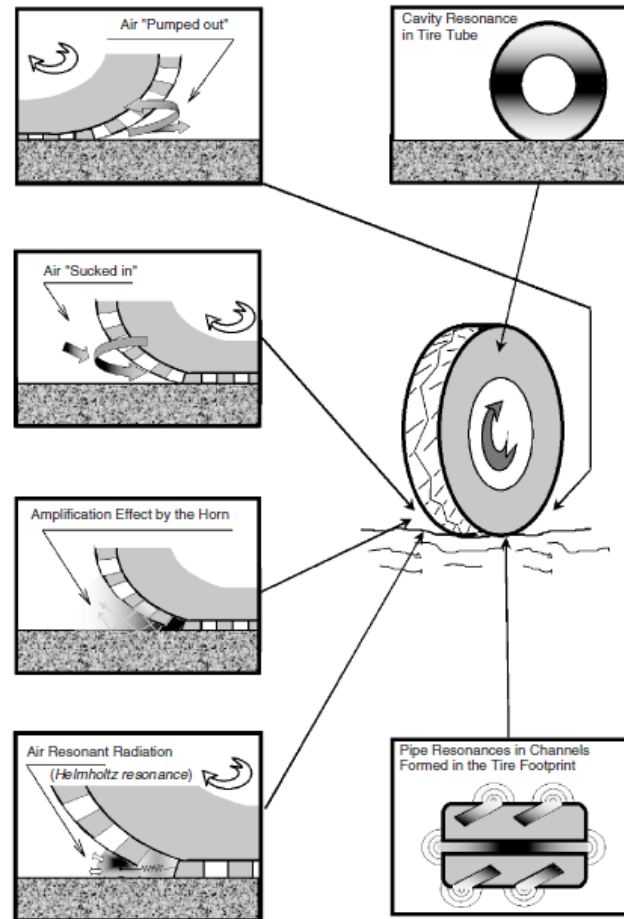


$$Q \propto \frac{d(\Delta V)}{dt}$$

The implosion of a cavitation bubble is a strong source of sound, because it occurs in a very short time span (Åbom, 2011).

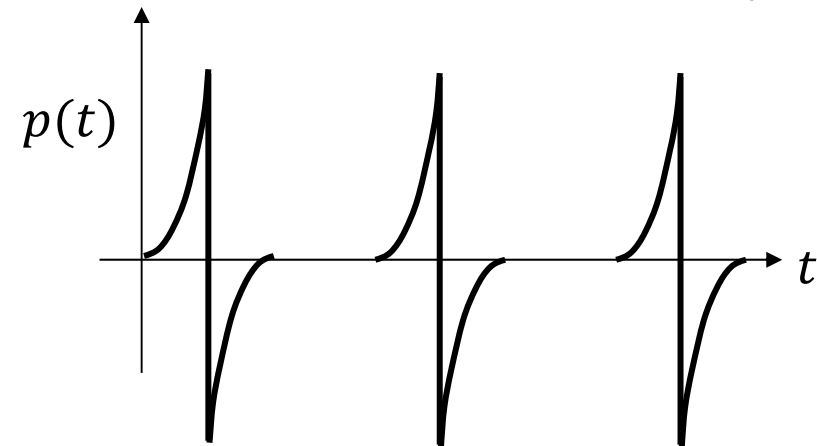
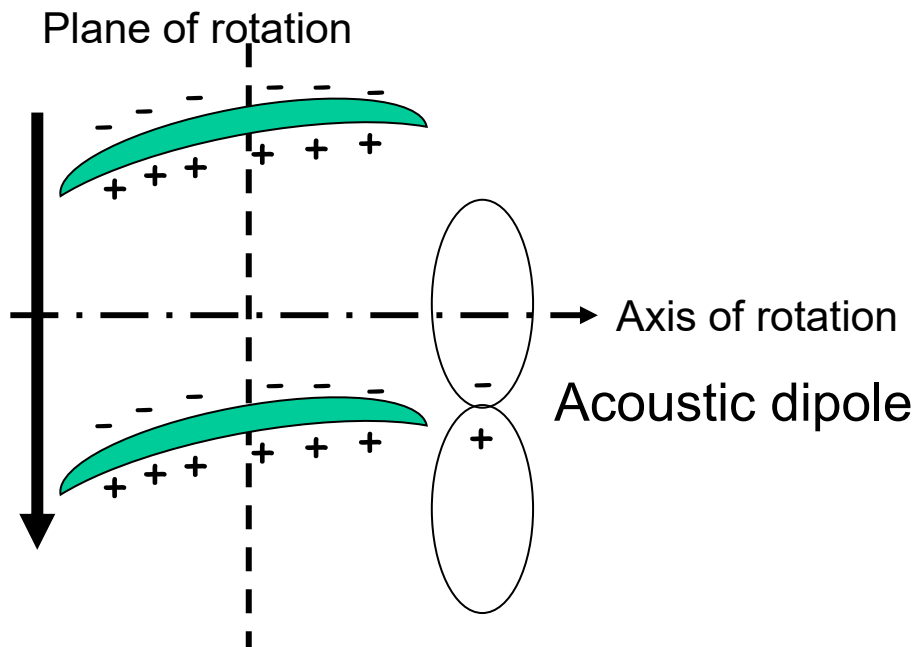


Flow Noise Sources Monopoles



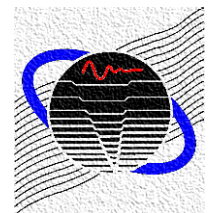
Flow Noise Sources **Dipoles**

- A fan blade is a moving airfoil
- Positive and negative pressures produce noise to a stationary observer



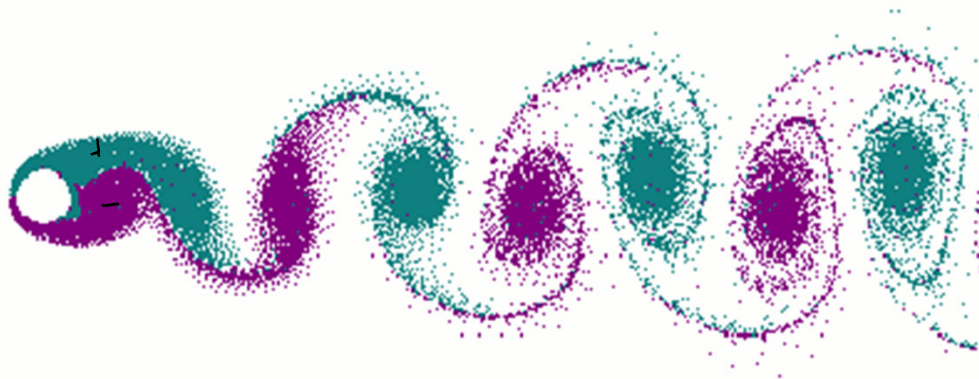
$$\rightarrow f_B = \left(\frac{N}{60}\right) B$$

B = number of blades

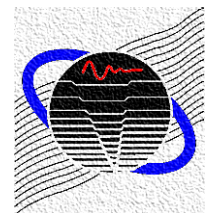
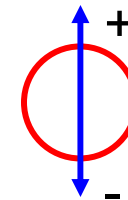


Flow Noise Sources **Dipoles**

Flow over a rod

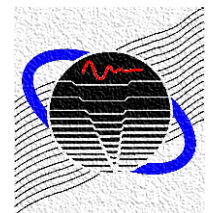
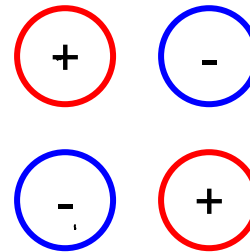
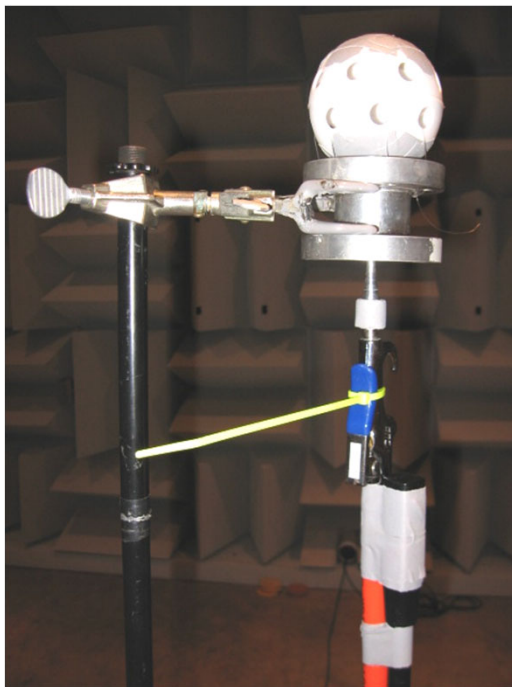


Oscillating



Flow Noise Sources **Quadrupoles**

Turbulence

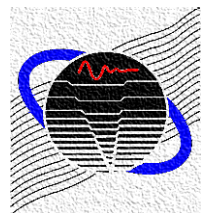


The Strouhal Frequency

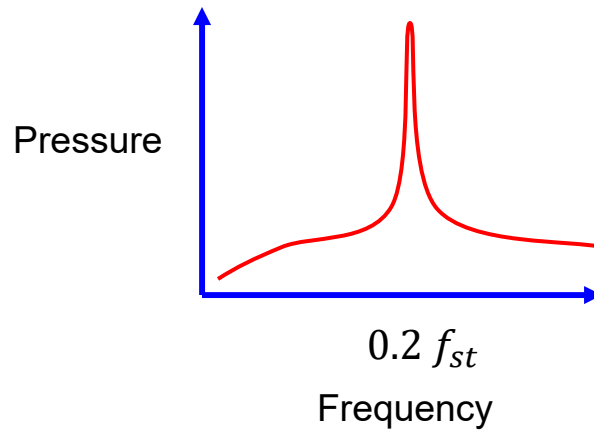
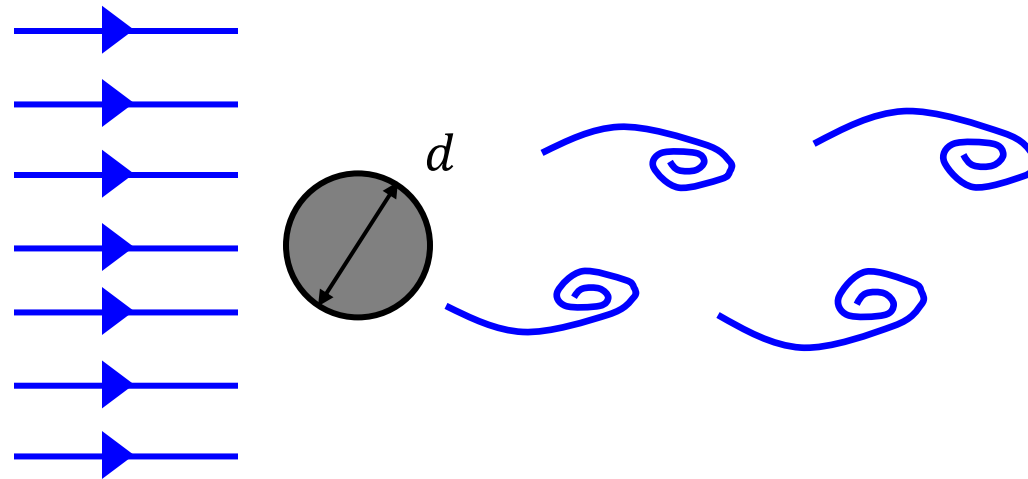
The frequency content scales to or is proportional to the Strouhal frequency.

$$f_{st} = \frac{U}{d}$$

Where d is the dimension of the source and U is the flow velocity.

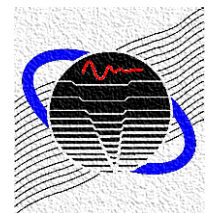


Case 1 Periodic Vortex Shedding

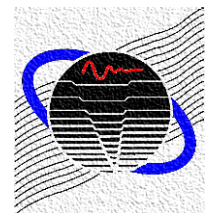
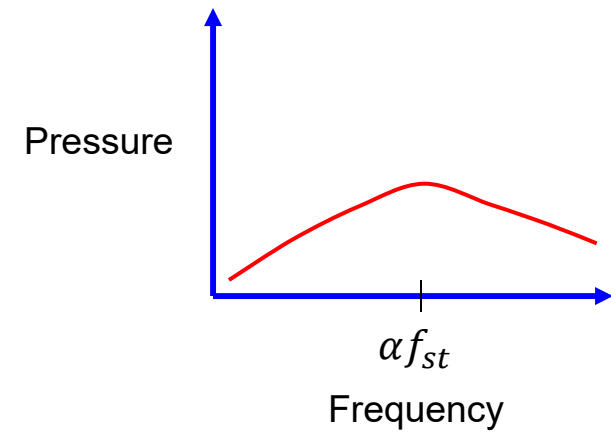
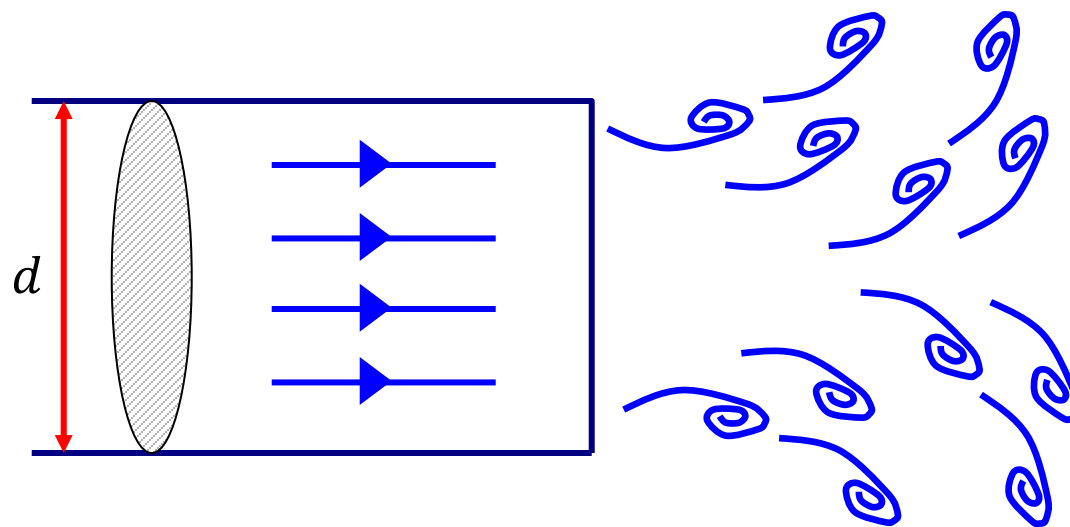


Vortex Shedding Frequency

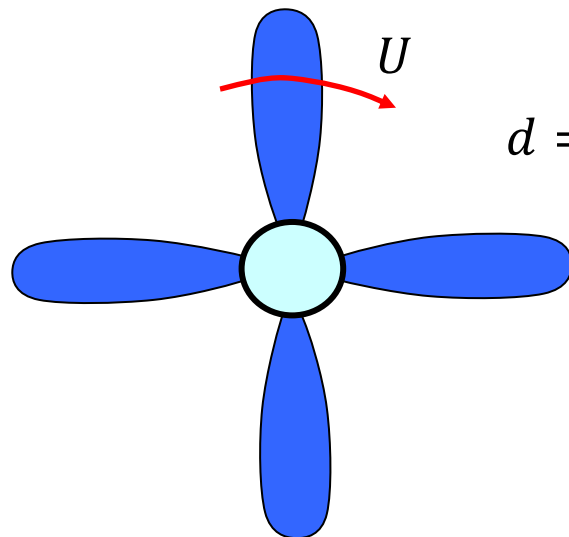
$$f_{vs} = \frac{0.2U}{d}$$



Case 2 Turbulent Jet

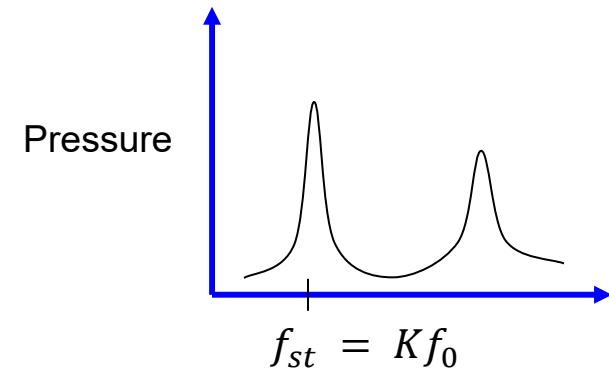


Case 3 Fan or Propeller

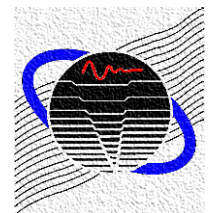


$$d = \frac{\pi D}{K}$$

$$f_{st} = \frac{U}{d} = \frac{\pi f_0 D}{\pi D / K}$$



Where D is the diameter of the source, K is the number of blades, and f_0 is the rotational frequency.



Case 4 Air Flow over Cavities

Rossiter's Equation (for Air)

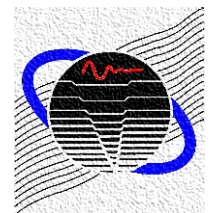
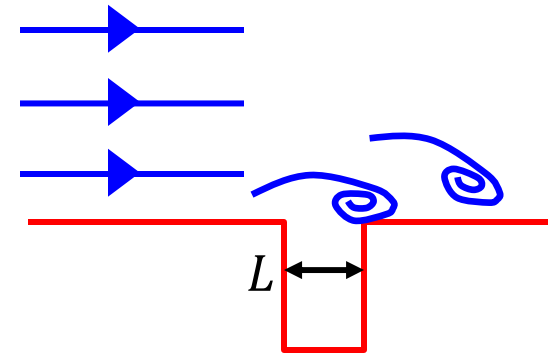
$$f_{vs} = \left(\frac{j - \gamma_R}{1/K_R + M} \right) \frac{U}{L} = \left(\frac{j - \gamma_R}{1/K_R + M} \right) f_{st}$$

L streamwise cavity length

$j = 1, 2, 3, \dots$ mode number

$\gamma_R = 0.25$ phase shift of acoustic scattering at downstream edge

$K_R = 0.61$ to 0.66 ratio of convective speed of the shear layer vortices to free stream velocity



Case 5 Whistle Tones

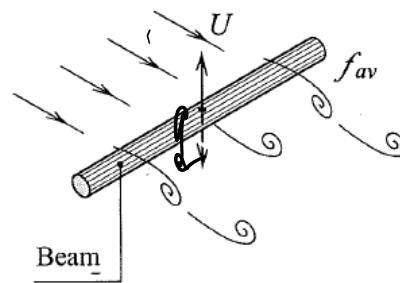
Vortex Shedding Frequency

$$f_{vs} = \alpha f_{st}$$

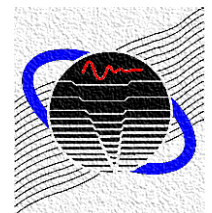
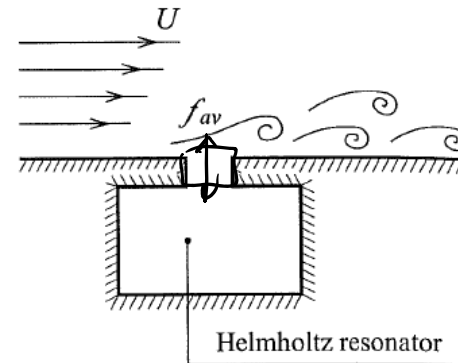
Self Excited Acoustic Oscillation

$$f_{vs} = f_{res}$$

Case I

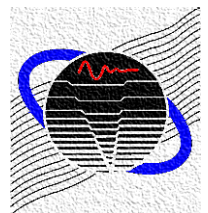


Case II



Objectives

- Applied overview of aeroacoustic sources
- **Scaling laws for sound power**
- Practical measures to avoid problems



Sound Power Relationships

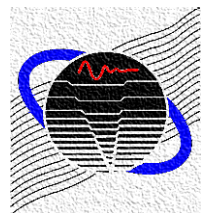
Relationship between a monopole and dipole

$$\frac{\bar{W}_{dipole}}{\bar{W}_{monopole}} = \frac{(kd)^2}{3}$$

Relationship between a dipole and quadrupole

$$\frac{\bar{W}_{quadrupole}}{\bar{W}_{dipole}} = \frac{(kd)^2}{5}$$

where d is the dimension of the source assuming the source region is assumed to be small compared to an acoustic wavelength.

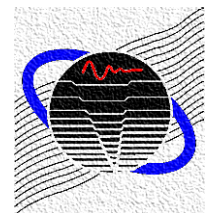


Size of the Source Region

$$kd = \left(\frac{2\pi f_{st}}{c} \right) d = \left(\frac{2\pi}{c} \right) \left(\frac{U}{d} \right) d = 2\pi M$$

Flow acoustic sources are acoustically small for small Mach (M) numbers.

$$\frac{\bar{W}_{dipole}}{\bar{W}_{monopole}} \propto M^2 \qquad \frac{\bar{W}_{quadrupole}}{\bar{W}_{dipole}} \propto M^2$$



Sound Power of a Monopole

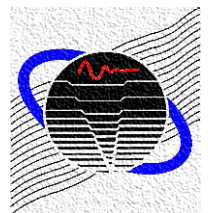
Sound power for a monopole

$$\bar{W}_m = \frac{\rho_0 c k^2}{4\pi} Q^2 \qquad k = \frac{2\pi f_{st}}{c} = \frac{2\pi(U)}{c(d)}$$

Where the volume velocity (Q) is $Q \propto U d^2$ Speed \times Area

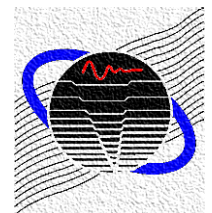
$$\bar{W}_m \propto \frac{\rho_0 c}{4\pi} \left(\frac{2\pi U}{c} \frac{U}{d} \right)^2 (U d^2)^2$$

$$\bar{W}_m \propto \rho_0 d^2 \frac{U^4}{c} = \rho_0 d^2 U^3 M$$



Scaling Laws for Sound Power

Dimension	Monopole	Dipole	Quadrupole
1-D	$\rho_0 c d^2 U^2$	$\rho_0 d^2 U^3 M$	$\rho_0 d^2 U^3 M^3$
2-D	$\rho_0 d^2 U^3$	$\rho_0 d^2 U^3 M^2$	$\rho_0 d^2 U^3 M^4$
3-D	$\rho_0 d^2 U^3 M$	$\rho_0 d^2 U^3 M^3$	$\rho_0 d^2 U^3 M^5$



Relative Importance of the Sources

Ordering Based on Mach Number

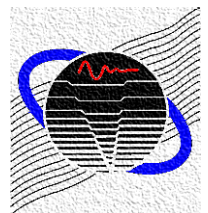
$$W_M : W_D : W_Q :: M : M^3 : M^5$$

Ordering Based on Flow Velocity (sources of same type)

$$W_M : W_D : W_Q :: U^4 : U^6 : U^8$$

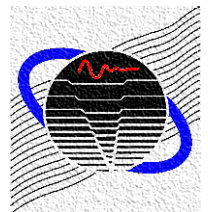
Ordering Based on Frequency

$$W_M : W_D : W_Q :: f : f^2 : f^4$$



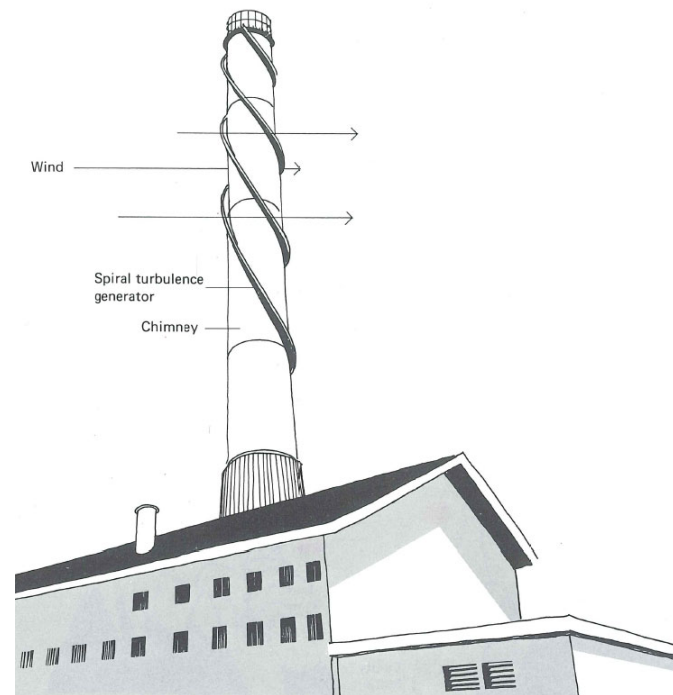
Objectives

- Applied overview of aeroacoustic sources
- Scaling laws for sound power
- Practical measures to avoid problems

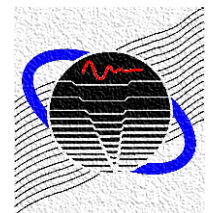


Prevention Vortex Shedding

Add spoilers to a smoke stack since the flow direction is variable.

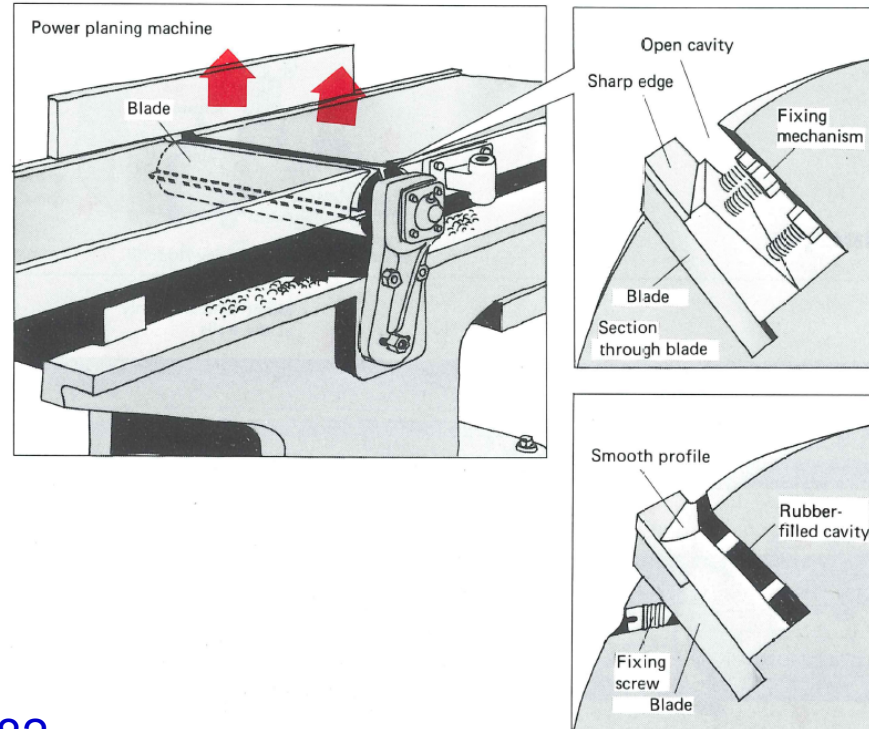


Brüel and Kjaer, 1982

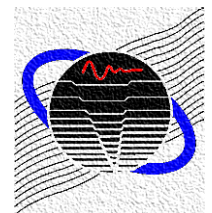


Prevention Air Flow over Cavities

1. Round the edges to reduce a whistle.
2. Fill cavities to avoid resonant amplification of sound.

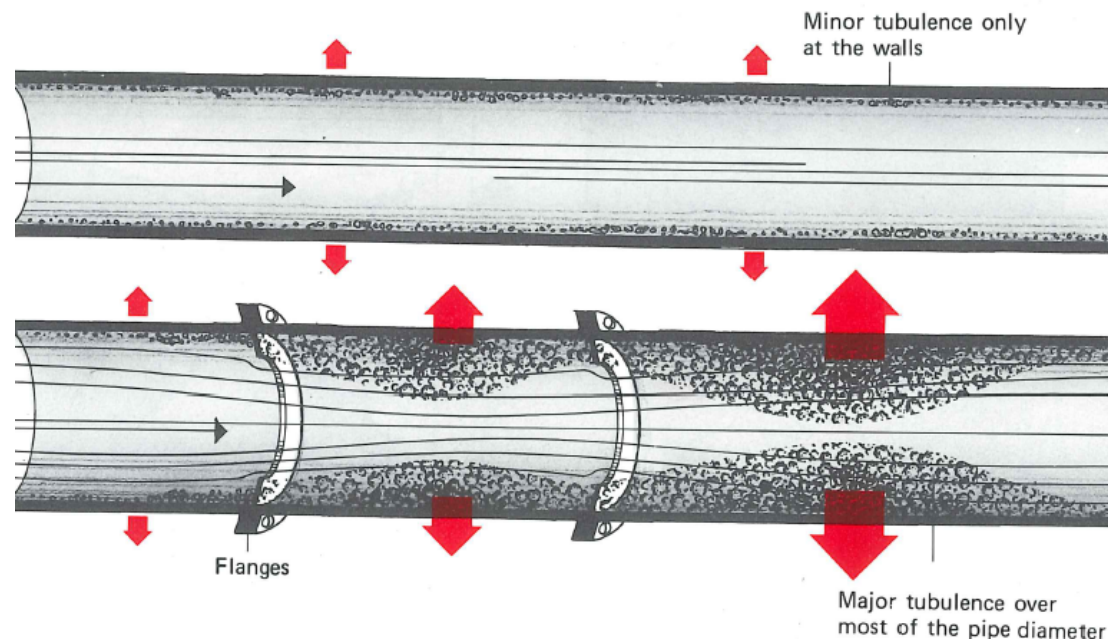


Brüel and Kjaer, 1982

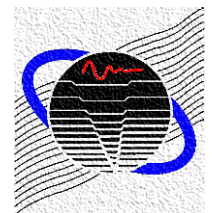


Prevention Turbulence in Pipes

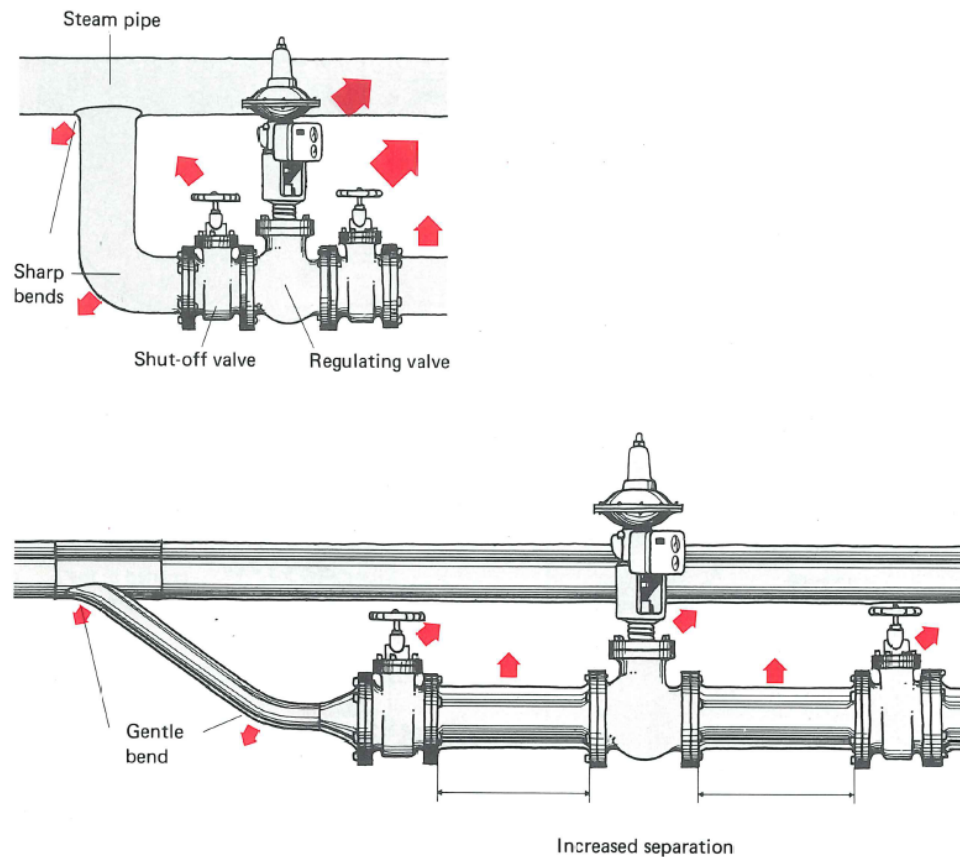
1. Avoid obstacles and sharp bends.
2. Add length to allow turbulence to settle.



Brüel and Kjaer, 1982

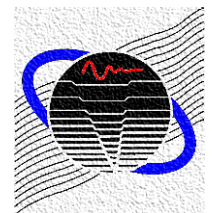


Prevention Turbulence in Pipes



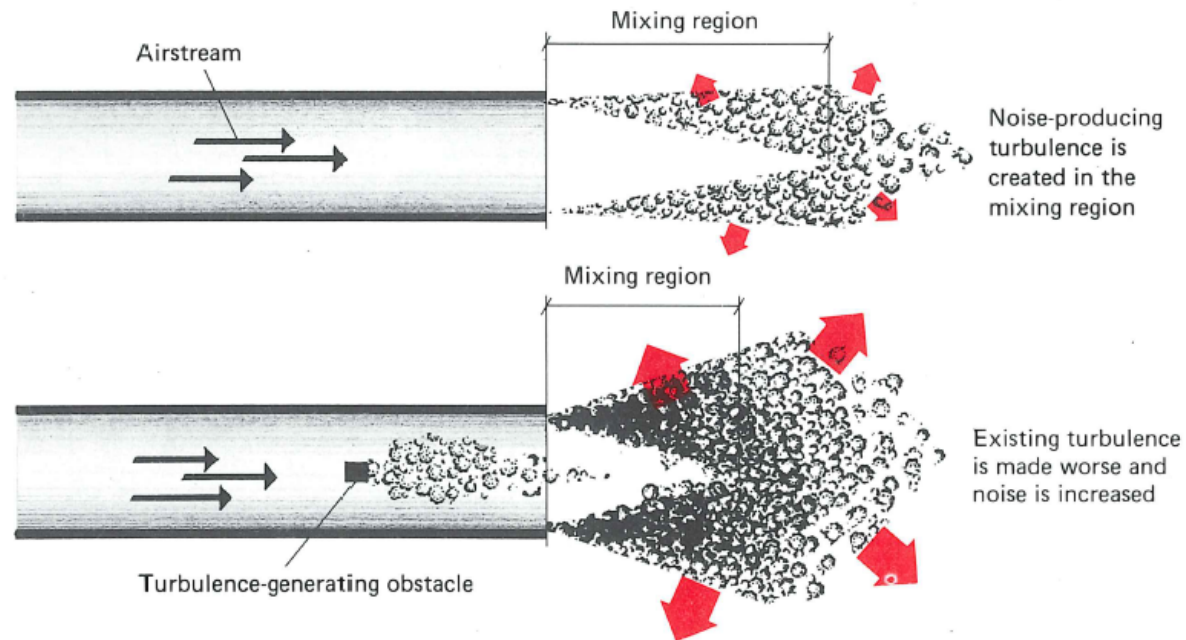
Brüel and Kjaer, 1982

Vibro-Acoustics Consortium

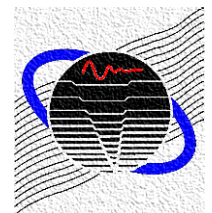


Prevention Exhaust Noise

1. Avoid obstacles in the flow (can amplify sound up to 20 dB).
2. Halving the speed leads to a noise reduction of about 15 dB.

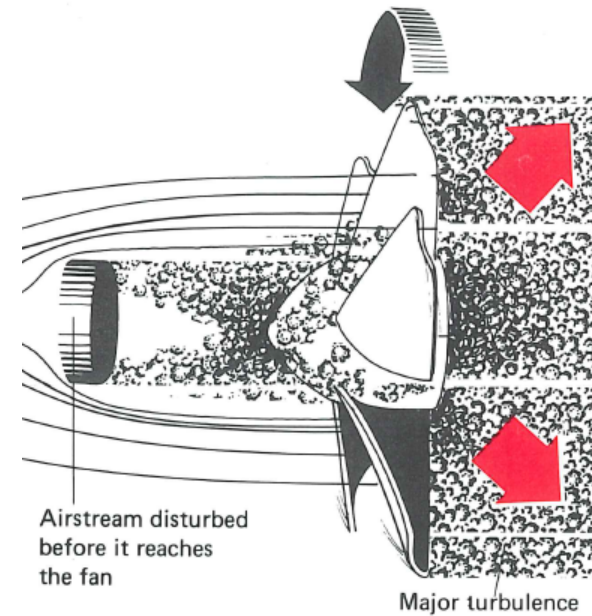
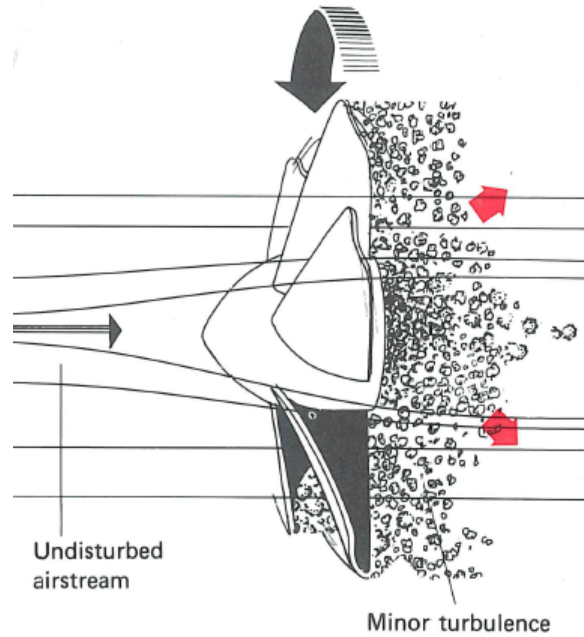


Brüel and Kjaer, 1982



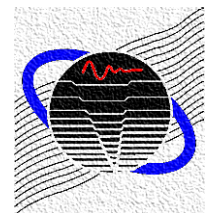
Prevention Fan Noise

Place fans well downstream of obstacles or bends.

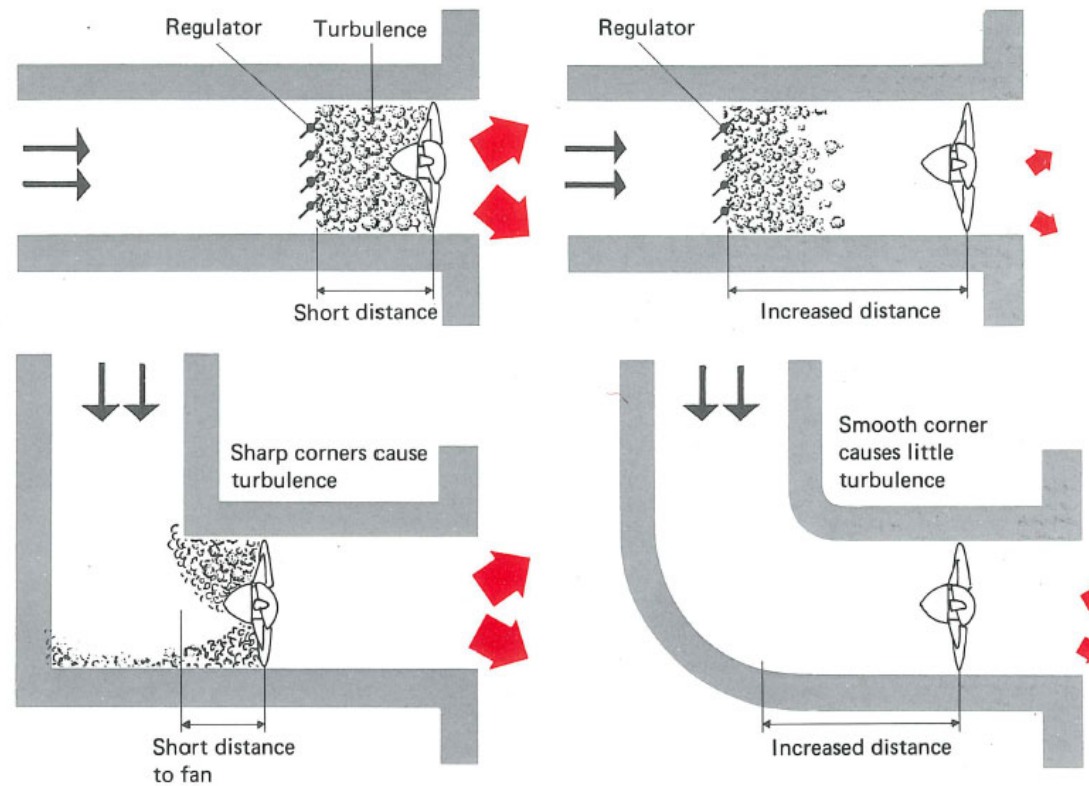


Brüel and Kjaer, 1982

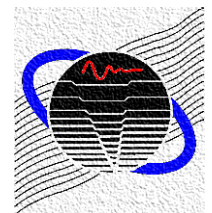
Vibro-Acoustics Consortium



Prevention Fan Noise

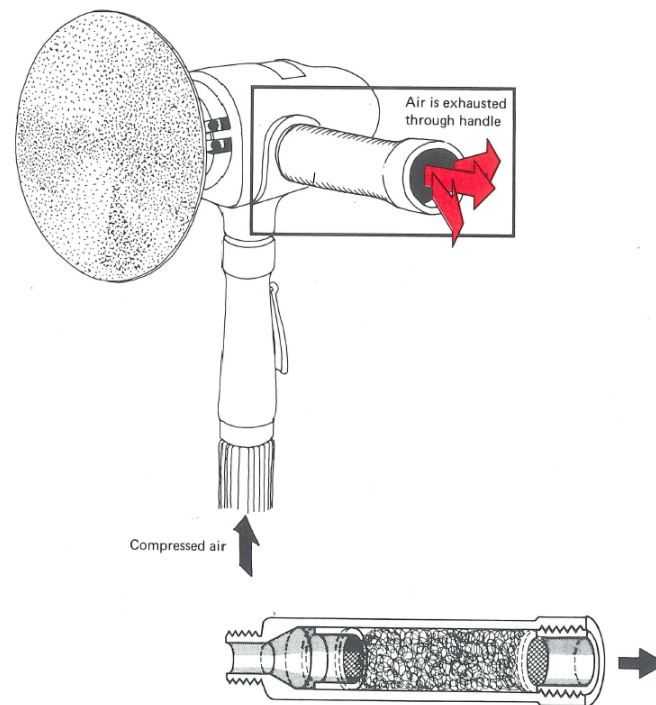


Brüel and Kjaer, 1982

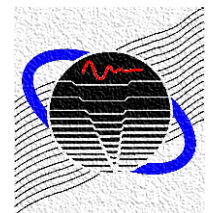


Prevention Exhaust Noise

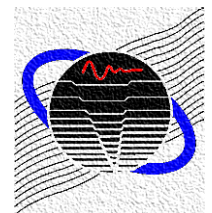
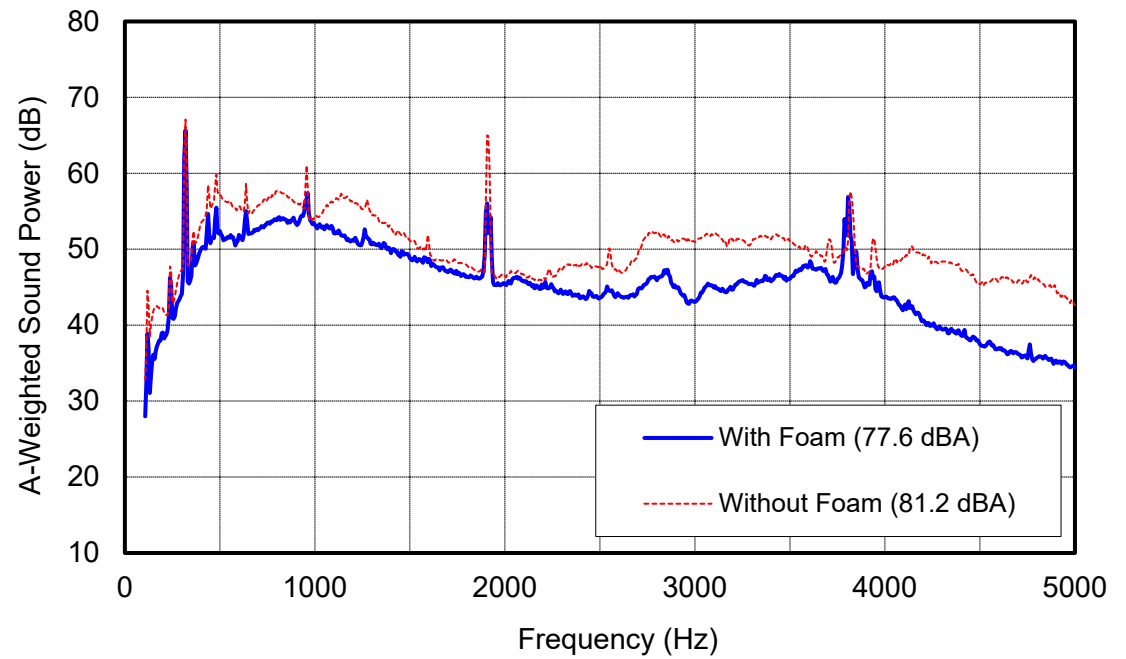
Add absorption in pipe to smooth turbulence and absorb sound.



Brüel and Kjaer, 1982

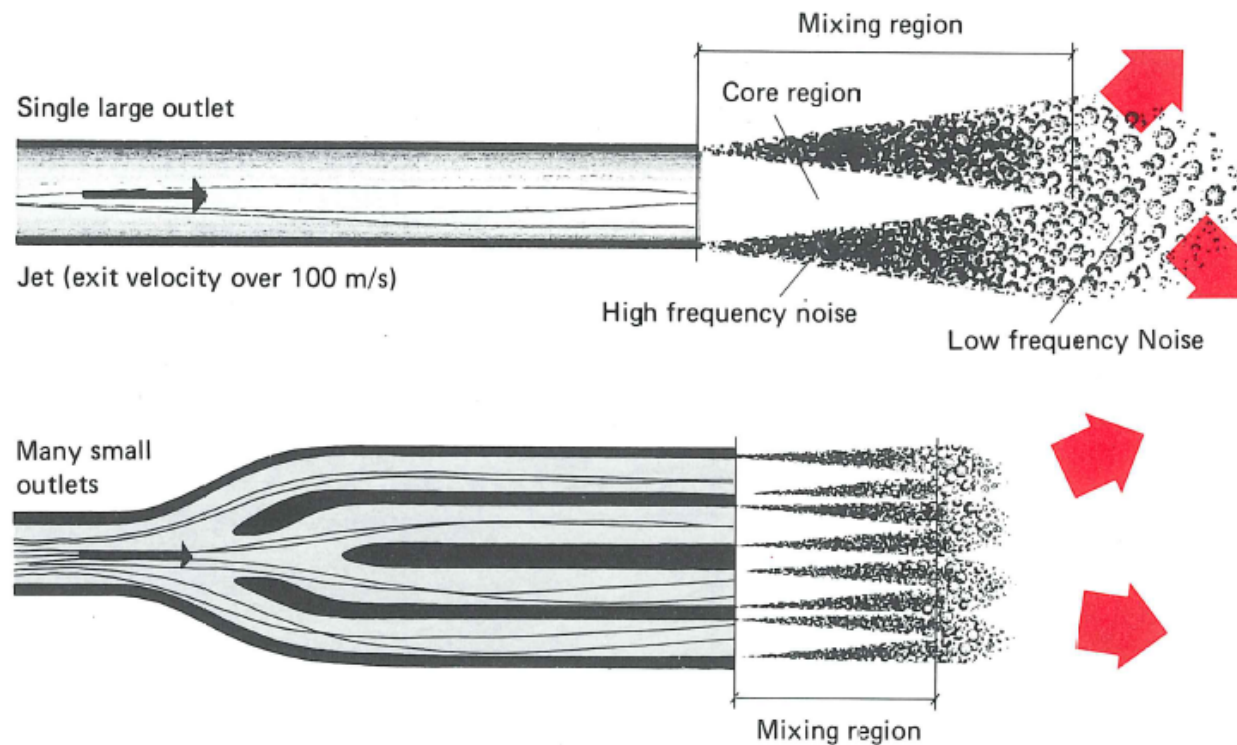


Prevention Exhaust Noise

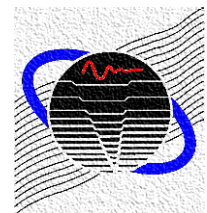


Prevention Exhaust Noise

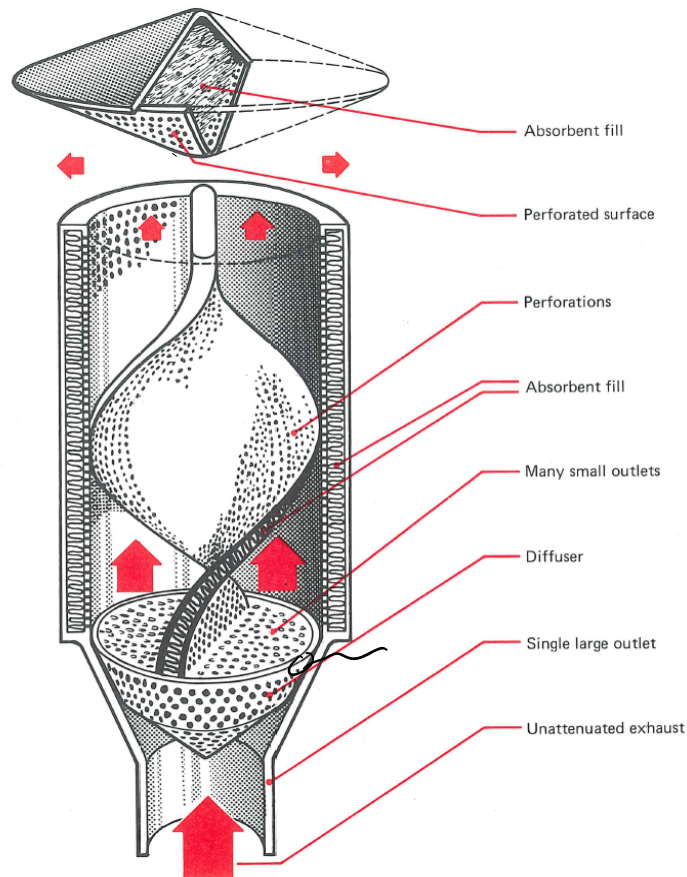
Replace a large exhaust by a number of small pipes.



Brüel and Kjaer, 1982

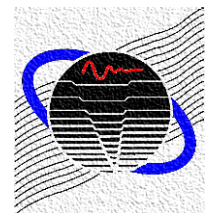


Prevention Exhaust Noise



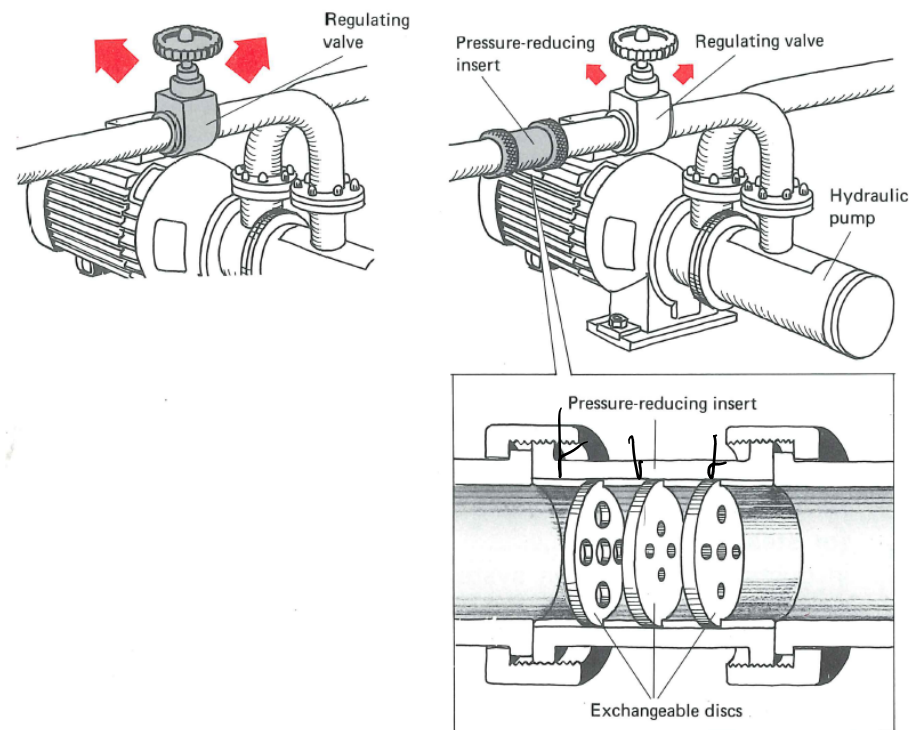
Change the noise problem from low to high frequency so that absorption can be used to attenuate the sound.

Brüel and Kjaer, 1982

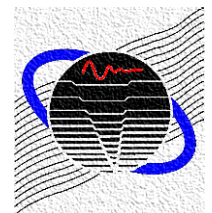


Prevention Cavitation

Lower pressures in a number of small steps.



Brüel and Kjaer, 1982



References

- ✓ H. P. Wallin, U. Carlsson, M. Åbom, H. Bodén, and R. Glav, "Chapter 8: Sound Generation and Radiation," Sound and Vibration, Marcus Wallenberg Laboratory, Stockholm (2011).
- ✓ Noise Control: Principles and Practice, Brüel and Kjaer, Denmark (1982).
<https://www.bksv.com/media/doc/bn1299.pdf>

