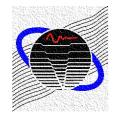
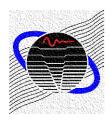
Impact Noise

Vibro-Acoustics Consortium Web Meeting
University of Kentucky



References

- ASTM E492 Standard Test Method for Laboratory Measurement of Impact Sound Transmission Through Floor-Ceiling Assemblies Using the Tapping Machine
- ASTM E989 Standard Classification for Determination of Single-Number Metrics for Impact Noise
- ASTM E1007 Standard Test Method for Field Measurement of Tapping Machine Impact Sound Transmission Through Floor-Ceiling Assemblies and Associated Support Structures
- Standards are used to assess footfall noise.

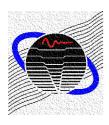


Standard Tapping Machine

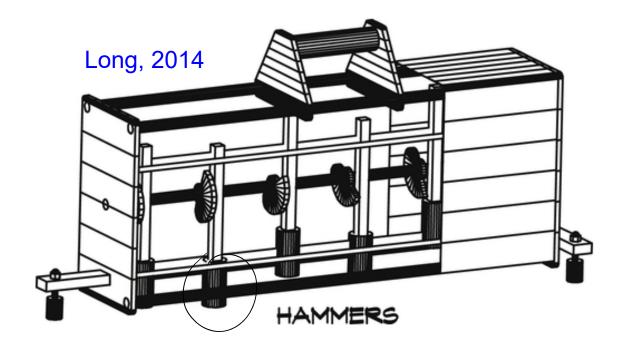
- A standard tapping machine is used to rate the impact noise isolation of floors in dwellings.
- Tapping machine consists of five hammers each weighing 500 g, and dropping from a height of 4 cm.
- Each impacts the surface at 2 Hz providing an operating frequency of 10 Hz.

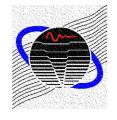
Brüel and Kjaer Type 3207



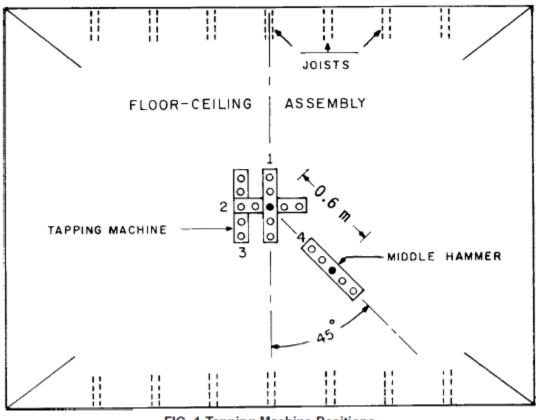


Standard Tapping Machine



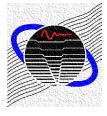


Tapping Machine Positions



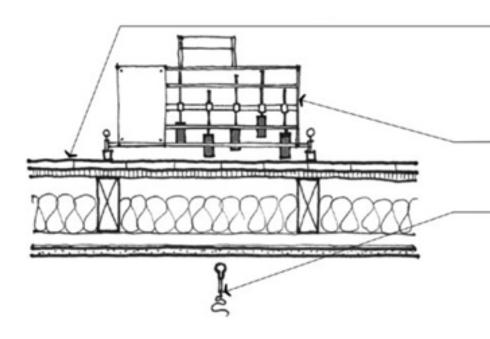
ASTM E1007





Impact Insulation Class Measurement

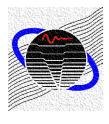
Ermann, 2015



For this example, we'll test the impact insulation class (IIC) of a wood-joist floor with a ceiling suspended from resilient channel. We wish to establish a single-number rating to compare the acoustical performance of assemblies in the attenuation of impact sound.

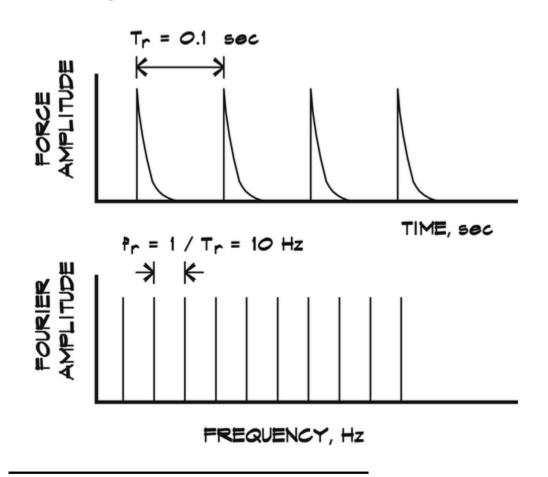
A tapping machine drops 10 steel hammers per second on the floor surface. (Five hammers each drop twice per second.)

 A microphone measures the impact sound pressure level (ISPL) in the room below the engaged tapping machine.



Tap Machine Signal

Long, 2014



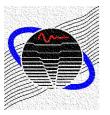
Fourier Amplitude

$$F_n \cong \frac{2}{T_r} \int_0^{T_r} f(t)dt = 2f_r m v_0$$

$$F_n \cong 2f_r m \sqrt{2gd}$$

d drop distance

m mass



Impact Insulation Class

The impact noise isolation capability of a floor

$$L_n = L_P - 10 \log \frac{A_0}{S\overline{\alpha}_{S,ab}}$$

where

 L_n normalized impact sound pressure level

 L_P 1/3-octave band sound pressure level as measured, dB

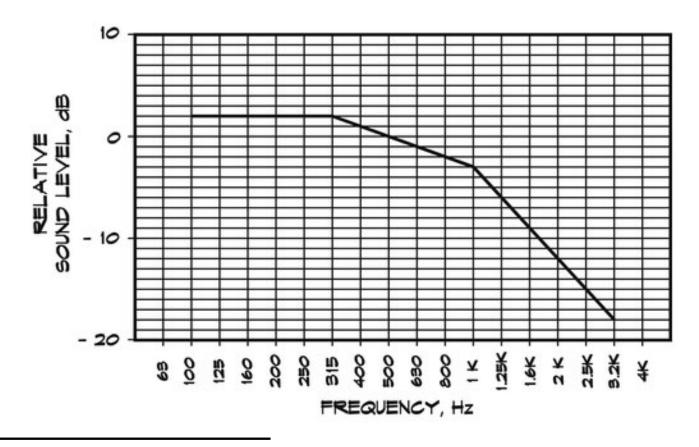
 $S\bar{\alpha}_{S,ab}$ total absorption in receiving room, m²

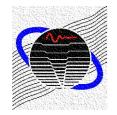
 A_0 reference value of absorption, 10 m²

For field measurements, California drops the second term on the right-hand side, so it is less strict.

Impact Insulation Class

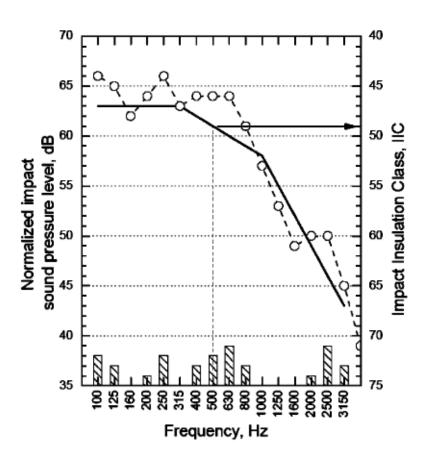
Reference contour for calculating impact insulation class (Long, 2014)





Impact Insulation Class

ASTM E989



The reference contour is shifted until

- the sum of positive differences is less than 32 dB.
- the maximum deficiency in a frequency band does not exceed 8 dB.

The normalized sound pressure level at 500 Hz is subtracted from 110 dB to obtain the impact insulation class (IIC).

Field IIC tests normally fall about five points below the laboratory test and apply only to the room in which they are measured. Receiving rooms should meet a minimum volume requirement.

Infinite Panel Expression

Fourier Amplitude

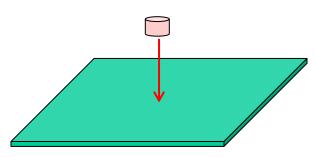
$$F_n \cong \frac{2}{T_r} \int_0^{T_r} f(t)dt = 2f_r m \sqrt{2gd}$$

d drop distance (40 mm)

m mass (500 grams)

 f_r impact frequency (10 Hz)

Assume infinite plate and perform power balance



$$L_n(\text{oct}) = 10 \log_{10} \left(\frac{4}{5.1} \frac{(\rho c)^2 \sigma_{rad}}{p_{ref}^2 A_0 \rho_m^2 c_L \eta h^3} \right)$$

 ρ_m density of panel (kg/m³)

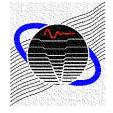
 E_m elastic modulus of panel (Pa)

 η loss factor of panel

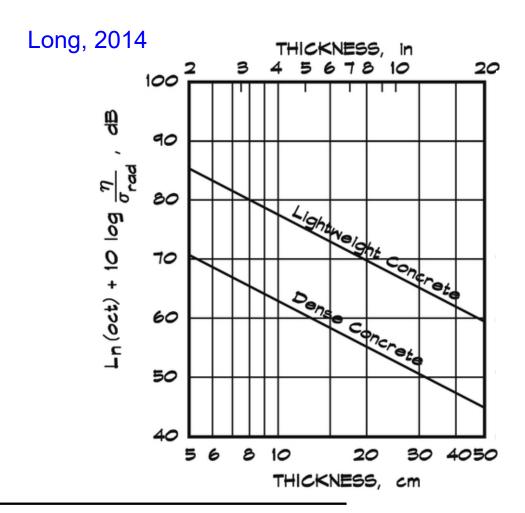
$$c_L = \sqrt{E/\rho_m}$$
 (m/s)

h plate thickness (m)

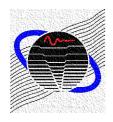
 σ_{rad} radiation efficiency $p_{ref}\cong 20 imes 10^{-6}$ Pa $A_0=10~{
m m}^2$



Infinite Panel Results

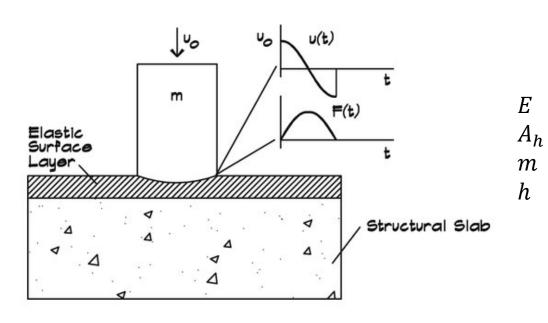


dB levels are typical of those using a tapping machine.



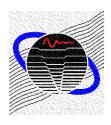
Add an Elastic Layer

Long, 2014



elastic modulus of layer area of hammer mass of hammer

thickness of layer



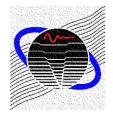
Add an Elastic Layer Improvement

$$\Delta L_n = 20 \log \left(\frac{4\pi}{\sin(\alpha)/\alpha + \sin(\beta)/\beta} \right)$$

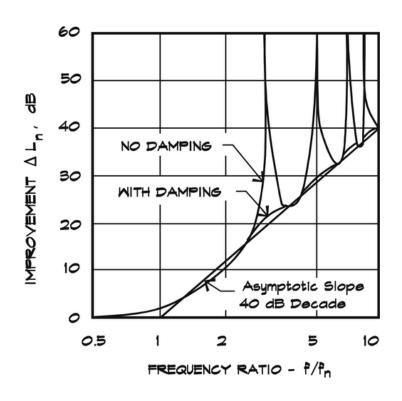
$$\alpha = \frac{\pi}{2} \left(1 - n \frac{f_r}{f_0} \right) \qquad \beta = \frac{\pi}{2} \left(1 + n \frac{f_r}{f_0} \right)$$

$$f_r = 10 \text{ Hz and } n = 1, 2, 3, ...$$

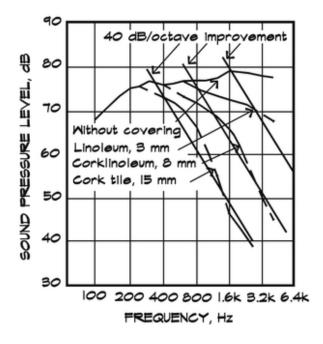
$$f_0 = \frac{1}{2\pi} \sqrt{\frac{A_h}{m}} \sqrt{\frac{E}{h}}$$

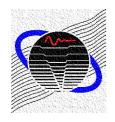


Add an Elastic Layer Improvement



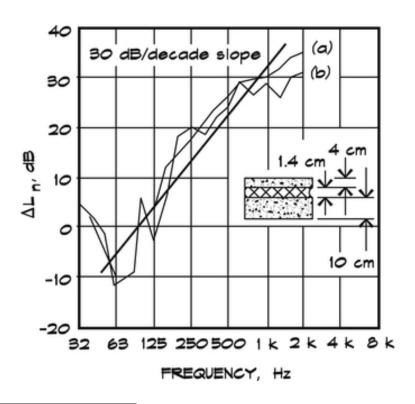
Footfall noise level under a 12 cm thick concrete floor with various floor coverings (Measured data by Cremer and Heckl, 1973)

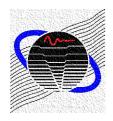




Resonantly Reacting Floating Floor

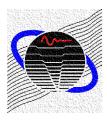
a) Standard tapping machine b) High-heeled shoes Note the negative $\Delta\,L_n\,$ in the vicinity of the resonant frequency.





Summary

- Building acousticians assume that impact noise is unavoidable.
- Standard tapping instrument is used to simulate the impact.
- Impact Insulation Class (IIC) is a standard way of assessing how readily impact noise is transmitted to the floor below.
- Impact noise can be reduced by increasing the thickness of the floor, adding an elastic layer, or using a floating floor.
- Perhaps similar ideas can be integrated into buzz and rattle assessment and mitigation.



Locally Reacting Floating Floor

Heavily Damped Floating Floor

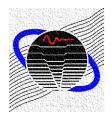
$$\Delta L_n = 20 \log \left[1 + \left(\frac{f}{f_0} \right)^2 \right] \approx 40 \log \frac{f}{f_0}$$

where

$$f_0 = \frac{1}{2\pi} \sqrt{\frac{k'}{\rho_{s_1}}}$$

k' dynamic stiffness per unit area

 ρ_{s_1} mass per unit area of floating slab



Resonantly Reacting Floating Floor

Lightly Damped Floating Floor

$$\Delta L_n(\omega) \approx 10 \log \left(2.3 \sqrt{\frac{E_m}{\rho_m}} h_1 \eta_1 n' \frac{\omega^3}{\omega_l^4} \right)$$

 h_1 thickness of floating slab, m

 E_m elastic modulus of floating slab

 ρ_m density of floating slab

 η_1 loss factor of floating slab

n' number of resilient mounts per unit area of slab, m^2

 ω_l resonant frequency of floating slab

